## GATE 2023

## Civil Engineering

## Afternoon Shift

## Questions with Detailed Solutions

## General Aptitude

1. The line ran $\qquad$ the page, right through the centre, and divided the page into two.
A. Across
B. of
C. Between
D. About
[MCQ - 1 Mark]
Ans. A
Sol. The line ran across the page, right through the centre, and divided the page into two.
2. Kind: $\qquad$ : : Often : Seldom
(By word meaning)
A. Cruel
B. Variety
C. Type
D. Kindred
[MCQ - 1 Mark]
Ans. A
Sol. Kind : Cruel : : Often : Seldom
Often means regular repetition.
Seldom means very rarely occurring.
Hence, often and seldom are the opposite.
The correct opposite of kind is cruel.
Kindred means similar or related.
3. In how many ways can cells in a $3 \times 3$ grid be shaded, such that each row and each column have exactly one shaded cell? An example of one valid shading is shown.
A. 2
B. 9
C. 3
D. 6

Ans. D
Sol.

$3 \times 2 \times 1=6$
4. There are 4 red, 5 green, and 6 blue balls inside a box. If $N$ number of balls are picked simultaneously, what is the smallest value of $N$ that guarantees there will be at least two balls of the same colour?
One cannot see the colour of the balls until they are picked.
A. 4
B. 15
C. 5
D. 2
[MCQ - 1 Mark]
Ans. A
Sol. 3 varieties of balls are there i.e. R, G \& B If we pick up 4 balls, one ball will repeat.
5. Consider a circle with its centre at the origin (O), as shown. Two operations are allowed on the circle.

Operation 1: Scale independently along the $x$ and $y$ axes.
Operation 2: Rotation in any direction about the origin.
Which figure among the options can be achieved through a combination of these two operations on the given circle?

A.

B.

C.

D.


Ans. A

## Sol.

> Operation 1:


Suppose $S_{x \text {-axis }}>S_{x \text {-axis }}$

Operation 2:

6. Elvesland is a country that has peculiar beliefs and practices. They express almost all their emotions by gifting flowers. For instance, if anyone gifts a white flower to someone, then it is always taken to be a declaration of one's love for that person. In a similar manner, the gifting of a yellow flower to someone often means that one is angry with that person.
Based only on the information provided above, which one of the following sets of statement(s) can be logically inferred with certainty?
(i) In Elvesland, one always declares one's love by gifting a white flower.
(ii) In Elvesland, all emotions are declared by gifting flowers.
(iii) In Elvesland, sometimes one expresses one's anger by gifting a flower that is not yellow.
(iv) In Elvesland, sometimes one expresses one's love by gifting a white flower.
A. only (ii)
B. (i), (ii) and (iii)
C. (i), (iii) and (iv)
D. only (iv)
[MCQ - 2 Marks]
Ans. D
7. Three husband-wife pairs are to be seated at a circular table that has six identical chairs. Seating arrangements are defined only by the relative position of the people. How many seating arrangements are possible such that every husband sits next to his wife?
A. 16
B. 4
C. 120
D. 720
[MCQ - 2 Marks]
Ans. C
Sol.


So, total no. $=2 \times 2 \times 2 \times 2$

8. Based only on the following passage, which one of the options can be inferred with certainty? When the congregation sang together, Apenyo would also join, though her little screams were not quite audible because of the group singing. But whenever there was a special number, trouble would begin; Apenyo would try singing along, much to the embarrassment of her mother. After two or three such mortifying Sunday evenings, the mother stopped going to church altogether until Apenyo became older and learnt to behave.
At home too, Apenyo never kept quiet; she hummed or made up silly songs to sing by herself, which annoyed her mother at times but most often made her become pensive. She was by now convinced that her daughter had inherited her love of singing from her father who had died unexpectedly away from home.
A. The mother was embarrassed about her daughter's singing at home.
B. The mother's feelings about her daughter's singing at home were only of annoyance.
C. The mother was not sure if Apenyo had inherited her love of singing from her father.
D. When Apenyo hummed at home, her mother tended to become thoughtful.
[MCQ - 2 Marks]
Ans. B
9. If $x$ satisfies the equation $4^{8^{x}}=256$, then $x$ is equal to $\qquad$ .
A. $\frac{1}{2}$
B. $\log _{16} 8$
C. $\frac{2}{3}$
D. $\log _{4} 8$
[MCQ - 2 Marks]
Ans. C
Sol.

10. Consider a spherical globe rotating about an axis passing through its poles. There are three points $P, Q$, and $R$ situated respectively on the equator, the north pole, and midway between the equator and the north pole in the northern hemisphere. LetP, Q , and R move with speeds $\mathrm{V}_{\mathrm{P}}, \mathrm{V}_{\mathrm{Q}}$ and $V_{R}$, respectively.
Which one of the following options is CORRECT?
A. $\mathrm{V}_{\mathrm{P}}<\mathrm{V}_{\mathrm{R}}<\mathrm{V}_{\mathrm{Q}}$
B. $\mathrm{V}_{\mathrm{P}}<\mathrm{V}_{\mathrm{Q}}<\mathrm{V}_{\mathrm{R}}$
C. $\mathrm{V}_{\mathrm{P}}<\mathrm{V}_{\mathrm{R}}<\mathrm{V}_{\mathrm{Q}}$
D. $\mathrm{V}_{\mathrm{P}}=\mathrm{V}_{\mathrm{R}} \neq \mathrm{V}_{\mathrm{Q}}$
[MCQ - 2 Marks]
Ans. C

## Civil Engineering

11. Let $\phi$ be a scalar field, and $u$ be a vector field. Which of the following identities is true for $\operatorname{div}(\phi u)$ ?
A. $\operatorname{div}(\phi u)=\phi \operatorname{div}(u)+u \operatorname{grad}(\phi)$
B. $\operatorname{div}(\phi u)=\phi \operatorname{div}(u)+u \times \operatorname{grad}(\phi)$
C. $\operatorname{div}(\phi u)=\phi \operatorname{grad}(u)+u \operatorname{grad}(\phi)$
D. $\operatorname{div}(\phi u)=\phi \operatorname{grad}(u)+u \times \operatorname{grad}(\phi)$
[MCQ - 1 Mark]
Ans. A
Sol. $\operatorname{div}(\varphi \mathrm{u})=\varphi \operatorname{div}(\mathrm{u})+\mathrm{u} . \operatorname{grad}(\varphi)$ is a special property of vector.
12. Which of the following probability distribution functions (PDFs) has the mean greater than the median?


A. Function 1
B. Function 2
C. Function 3
D. Function 4
[MCQ - 1 Mark]
Ans. B
Sol. For positively skewed PDF, mean > median (Function 2)
For negatively skewed PDF, mean < median (Function 3)
For symmetrical PDF, mean $=$ median (Function 1)
13. A remote village has exactly 1000 vehicles with sequential registration numbers starting from 1000. Out of the total vehicles, $30 \%$ are without pollution clearance certificate. Further, evenand odd-numbered vehicles are operated on even-and odd-numbered dates, respectively.
If 100 vehicles are chosen at random on an even-numbered date, the number of vehicles expected without pollution clearance certificate is $\qquad$ -.
A. 15
B. 30
C. 50
D. 70
[MCQ - 1 Mark]
Ans. B
Sol. Since $30 \%$ of the total vehicles are without pollution clearance certificate.
$\therefore$ The number of vehicles expected without pollution clearance certificate out of 100 vehicles,

$$
\begin{aligned}
& =100 \times 0.3 \\
& =30
\end{aligned}
$$

14. A circular solid shaft of span $L=5 \mathrm{~m}$ is fixed at one end and free at the other end. A torque $T=$ $100 \mathrm{kN} . \mathrm{m}$ is applied at the free end. The shear modulus and polar moment of inertia of the section are denoted as $G$ and J, respectively. The torsional rigidity $G J$ is $50,000 \mathrm{kN} . \mathrm{m} 2 / \mathrm{rad}$. The following are reported for this shaft:
Statement-I: The rotation at the free end is 0.01 rad
Statement-II: The torsional strain energy is $1.0 \mathrm{kN} . \mathrm{m}$
With reference to the above statements, which of the following is true?
A. Both the statements are correct
B. Statement (I) is correct, but Statement II) is wrong
C. Statement (I) is wrong, but Statement II) is correct
D. Both the statements are wrong
[MCQ - 1 Mark]
Ans. B

## Sol. Given

Length of shaft $=5 \mathrm{~m}$, Applied torque $=100 \mathrm{kNm}$, Torsional Rigidity $=50,000 \mathrm{kN} . \mathrm{m}^{2} / \mathrm{rad}$

## Statement-I

Rotation at the free end $(\theta)=\frac{\tau \mathrm{L}}{\mathrm{GJ}}=\frac{100 \times 5}{50,000}=0.01 \mathrm{rad}$

## Statement -II

Torsional strain energy $=\frac{1}{2} \times T \times \theta=\frac{1}{2} \times 100 \times 0.01=0.5 \mathrm{kN} / \mathrm{m}$.
15. M20 concrete as per IS 456: 2000 refers to concrete with a design mix having $\qquad$
A. an average cube strength of 20 MPa
B. an average cylinder strength of 20 MPa
C. a 5 -percentile cube strength of 20 MPa
D. a 5-percentile cylinder strength of 20 MPa
[MCQ - 1 Mark]
Ans. C
Sol. M20 concrete as per IS 456:2000 refers to the concrete with a design mix having a 5-percentile cube strength of 20 MPa .
16. When a simply-supported elastic beam of span $L$ and flexural rigidity $E I$ ( $E$ is the modulus of elasticity and I is the moment of inertia of the section) is loaded with a uniformly distributed load w per unit length, the deflection at the mid-span is $\Delta_{0}=\frac{5}{384} \frac{\mathrm{wL}^{4}}{\mathrm{EI}}$.

If the load on one half of the span is now removed, the mid-span deflection $\qquad$ .
A. reduces to $\Delta_{0} / 2$
B. reduces to a value less than $\Delta_{0} / 2$
C. reduces to a value greater than $\Delta_{0} / 2$
D. remains unchanged at $\Delta_{0}$
[MCQ - 1 Mark]
Ans. A
Sol.


Total deflection due to loading on entire span $=$ Deflection due to load on left half + deflection due to load on right half

Total deflection on SSB due to UDL over the entire span $\Delta_{0}=\frac{5}{384} \frac{\mathrm{WL}^{4}}{\mathrm{EI}}$
Deflection due to half portion loading. $\Delta^{\prime}=\frac{\Delta_{0}}{2}=\frac{1}{2}\left(\frac{5}{384} \frac{\mathrm{WL}^{4}}{\mathrm{EI}}\right)$
So, midspan deflection reduced to $\Delta 0 / 2$
17. Muller-Breslau principle is used in analysis of structures for $\qquad$ .
A. drawing an influence line diagram for any force response in the structure
B. writing the virtual work expression to get the equilibrium equation
C. superposing the load effects to get the total force response in the structure
D. relating the deflection between two points in a member with the curvature diagram in-between
[MCQ - 1 Mark]
Ans. A
Sol. Muller-Breslau principle is used to draw ILD for any force response in the structure.
18. A standard penetration test (SPT) was carried out at a location by using a manually operated hammer dropping system with $50 \%$ efficiency. The recorded SPT value at a particular depth is 28. If an automatic hammer dropping system with $70 \%$ efficiency is used at the same location, the recorded SPT value will be $\qquad$ _.
A. 28
B. 20
C. 40
D. 25
[MCQ - 1 Mark]
Ans. $B$
Sol. Efficiency $(\eta) \propto \frac{1}{\operatorname{SPT} \text { value }(N)}$

$$
\begin{aligned}
& \eta \times N=\text { constant } \\
& \eta_{1} \times N_{1}=\eta_{2} \times N_{2} \\
& 0.3 \times 28=0.7 \times N_{2} \\
& N_{2}=20
\end{aligned}
$$

19. A vertical sheet pile wall is installed in an anisotropic soil having coefficient of horizontal permeability, $\mathrm{k}_{H}$ and coefficient of vertical permeability, kv . In order to draw the flow net for the isotropic condition, the embedment depth of the wall should be scaled by a factor of $\qquad$ —, without changing the horizontal scale.
A. $\sqrt{\frac{k_{H}}{k_{V}}}$
B. $\sqrt{\frac{\mathrm{k}_{\mathrm{V}}}{\mathrm{k}_{\mathrm{H}}}}$
C. 1.0
D. $\sqrt{\frac{k_{H}}{k_{V}}}$
[MCQ - 1 Mark]
Ans. A
Sol. As we know to change the horizontal distance in an anisotropic medium,

$$
X_{T}=X \sqrt{\frac{k_{\mathrm{V}}}{\mathrm{k}_{\mathrm{H}}}}
$$

But as per the question we cannot change the horizontal scale, hence we have to change the vertical length. So, we have to multiply depth with $\sqrt{\frac{\mathrm{k}_{\mathrm{H}}}{\mathrm{k}_{\mathrm{v}}}}$ to get the desired result.

Note: In the question, first they have mentioned soil as anisotropic then asked for isotropic condition. To transform the depth, we have to multiply $\sqrt{\frac{\mathrm{k}_{\mathrm{H}}}{\mathrm{k}_{\mathrm{V}}}}$. In isotropic conditions, $\mathrm{k}_{H}=\mathrm{k}_{\mathrm{v}}$, hence the factor becomes 1 . So, the correct answer can be $A$ and $C$.
20. Identify the cross-drainage work in the figure.

A. Super passage
B. Aqueduct
C. Siphon aqueduct
D. Level crossing
ing

[MCQ - 1 Mark]
Ans. A
Sol. Cross drainage works where the bed level of the stream is sufficiently above the FSL of canal is called super-passage.
21. Which one of the following options provides the correct match of the terms listed in Column-1 and Column-2?

| Column-1 |  | Column-2 |  |
| :---: | :---: | :---: | :---: |
| P | Horton equation | I | Precipitation |
| Q | Muskingum method | II | Flood frequency |
| R | Penman method | III | Evapotranspiration |
|  |  | IV | Infiltration |
|  |  | V | Channel routing |

A. P-IV, Q-V, R-III
B. P-III, Q-IV, R-I
C. P-IV, Q-III, R-II
D. P-III, Q-I, R-IV
[MCQ - 1 Mark]

Ans. A
Sol. Horton's equation $\rightarrow$ used in Infiltration calculation.
Muskingum method $\rightarrow$ used in channel routing.
Penman's equation $\rightarrow$ used in evapotranspiration calculation.
22. In the context of Municipal Solid Waste Management, 'Haul' in 'Hauled Container System operated in conventional mode' includes the $\qquad$ .
A. time spent by the transport truck at the disposal site
B. time spent by the transport truck in traveling between a pickup point and the disposal site with a loaded container
C. time spent by the transport truck in picking up a loaded container at a pickup point
D. time spent by the transport truck in driving from the depot to the first pickup point
[MCQ - 1 Mark]
Ans. B
Sol. 'Haul' in 'Hauled Container System operated in conventional mode' includes the time spent by the transport truck in traveling between a pickup point and the disposal site with a loaded container. The time spent at the disposal site isn't included in this.
23. Which of the following is equal to the stopping sight distance?
A. (braking distance required to come to stop) + (distance travelled during the perceptionreaction time)
B. (braking distance required to come to stop) - (distance travelled during the perceptionreaction time)
C. (braking distance required to come to stop)
D. (distance travelled during the perception-reaction time)
[MCQ - 1 Mark]
Ans. A
Sol.


SSD = Lag Distance + Breaking Distance
Breaking Distance = Braking distance required to come to stop
Lag Distance $=$ Distance travelled during the perception-reaction time
24. The magnetic bearing of the sun for a location at noon is $183^{\circ} 30^{\prime}$. If the sun is exactly on the geographic meridian at noon, the magnetic declination of the location is.
A. $3^{\circ} 30^{\prime} \mathrm{W}$
B. $3^{\circ} 30^{\prime} \mathrm{E}$
C. $93^{\circ} 30^{\prime} \mathrm{W}$
D. $93^{\circ} 30^{\prime} \mathrm{E}$
[MCQ - 1 Mark]
Ans. A
Sol. When the sun is exactly on the geographic meridian at noon, True bearing $=180^{\circ}$
Now, Magnetic Declination = True bearing - Magnetic bearing

$$
\begin{aligned}
& =180^{\circ}-183^{\circ} 30^{\prime} \\
& =-3^{\circ} 30^{\prime}=3^{\circ} 30^{\prime} \mathrm{W}
\end{aligned}
$$

25. For the matrix

$$
[A]=\left[\begin{array}{ccc}
1 & -1 & 0 \\
-1 & 2 & -1 \\
0 & -1 & 1
\end{array}\right]
$$

which of the following statements is/are TRUE?
A. $[A]\{x\}=\{b\}$ has a unique solution
B. $[A]\{x\}=\{b\}$ does not have a unique solution
C. [A] has three linearly independent eigenvectors
D. $[A]$ is a positive definite matrix
[MSQ - 1 Mark]

## Ans. B, C

Sol.

$$
\begin{aligned}
& |A-\lambda| \mid=0 \\
& {\left[\begin{array}{ccc}
1-\lambda & -1 & 0 \\
-1 & 2-\lambda & -1 \\
0 & -1 & 1-\lambda
\end{array}\right]=0} \\
& (1-\lambda)[(2-\lambda)(1-\lambda)-1]+1[\lambda-1]=0 \\
& (1-\lambda)[(2-\lambda)(1-\lambda)-1-1]=0 \\
& \lambda(1-\lambda)(3-\lambda)=0 \\
& \lambda=0,1,3
\end{aligned}
$$

As there are three eigen values so number of linearly independent eigenvectors are 3 .
Since, $|A|=0$
So, $[A]\{x\}=\{b\}$ does not have a unique solution
Now, for a positive matrix, all the eigenvalues of the matrix have to be positive but one of the $\lambda$ $=0$. So, $[A]$ is not a positive definite matrix.
26. In the frame shown in the figure (not to scale), all four members ( $A B, B C, C D$, and $A D$ ) have the same length and same constant flexural rigidity. All the joints $A, B, C$, and $D$ are rigid joints. The midpoints of $A B, B C, C D$, and $A D$, are denoted by $E, F, G$, and $H$, respectively. The frame is in unstable equilibrium under the shown forces of magnitude $P$ acting at E and G . Which of the following statements is/are TRUE?

A. Shear forces at H and F are zero
B. Horizontal displacements at H and F are zero
C. Vertical displacements at H and F are zero
D. Slopes at E, F, G, and H are zero

Ans. A, B and D
Sol. BMD for symmetrical box frame-


At H and $\mathrm{F}, \mathrm{BM}$ is constant.
$\Rightarrow S F=0$ (option A is correct)
Deflection diagram for symmetrical box frame


From the diagram, it is clear that-
$\rightarrow \delta_{v}$ at $H$ and $F \neq 0$ (option $B$ is incorrect)
$\rightarrow \theta$ at $\mathrm{E}, \mathrm{F}, \mathrm{G}, \mathrm{H}=0$ (option C is correct)
$\rightarrow \delta_{H}$ at $H$ and $F=0$ (option $D$ is correct)
27. With regard to the shear design of RCC beams, which of the following statements is/are TRUE?
A. Excessive shear reinforcement can lead to compression failure in concrete
B. Beams without shear reinforcement, even if adequately designed for flexure, can have brittle failure
C. The main (longitudinal) reinforcement plays no role in the shear resistance of beam
D. As per IS456:2000, the nominal shear stress in the beams of varying depth depends on both the design shear force as well as the design bending moment
[MSQ - 1 Mark]
Ans. A, B and D

## Sol.

1. Excessive shear reinforcement can cause compressive failure in concrete. So, option $A$ is correct.
2. Beams need to be provided with minimum shear reinforcement to avoid brittle failure. So, option B is correct.
3. Design shear strength of concrete $T_{c}$ (without shear reinforcement) depends upon-
(i) grade of concrete
(ii) \% main reinforcement

So, option C is incorrect.
4. Nominal shear stress for beam of varying depth, $\tau_{v_{u}}=\frac{V_{u}+\frac{M_{u}}{d} \tan \beta}{\text { B.d }}$
where, $\mathrm{V}_{\mathrm{u}}=$ design shear force
$M_{u}=$ design bending moment
So, option D is correct.
28. The reason(s) of the nonuniform elastic settlement profile below a flexible footing, resting on a cohesionless soil while subjected to uniform loading, is/are:
A. Variation of friction angle along the width of the footing
B. Variation of soil stiffness along the width of the footing
C. Variation of friction angle along the depth of the footing
D. Variation of soil stiffness along the depth of the footing

Ans. A, B and D
Sol. For a flexible footing placed on cohesionless soil, the variation of soil stiffness along the width of the footing results in a non-uniform settlement of the footing.
29. Which of the following is/are NOT active disinfectant(s) in water treatment?
A. OH (hydroxyl radical)
B. $\mathrm{O}_{3}$ (ozone)
C. $\mathrm{OCl}^{-}$(hypochlorite ion)
D. $\mathrm{Cl}^{-}$(chloride ion)
[MSQ - 1 Mark]
Ans. D
Sol. Hydroxyl radicals are highly reactive and can destroy pathogens quickly. Ozone \& hypochlorite ions are well-known disinfectants used to kill pathogens. However, chloride ions by themselves are not active disinfectants. They can help to stabilize and activate other disinfectants.
30. As per the Indian Roads Congress guidelines (IRC 86: 2018), extra widening depends on which of the following parameters?
A. Horizontal curve radius
B. Superelevation
C. Number of lanes
D. Longitudinal gradient
[MSQ - 1 Mark]
Ans. A, C
Sol. Extra widening $=\frac{n l^{2}}{2 R}+\frac{V}{9.5 \sqrt{R}}$
So extra widening depends on number of lane and radius.
31. The steady-state temperature distribution in a square plate $A B C D$ is governed by the 2dimensional Laplace equation. The side $A B$ is kept at a temperature of $100{ }^{\circ} \mathrm{C}$ and the other three sides are kept at a temperature of $0^{\circ} \mathrm{C}$. Ignoring the effect of discontinuities in the boundary conditions at the corners, the steady-state temperature at the center of the plate is obtained as $T_{0}{ }^{\circ} \mathrm{C}$. Due to symmetry, the steady-state temperature at the center will be same ( $\mathrm{T}_{0}{ }^{\circ} \mathrm{C}$ ), when any one side of the square is kept at a temperature of $100{ }^{\circ} \mathrm{C}$ and the remaining three sides are kept at a temperature of $0^{\circ} \mathrm{C}$. Using the principle of superposition, the value of $T_{0}$ is $\qquad$ (rounded off to two decimal places).
[NAT - 1 Mark]
Ans. 19.93

Sol. We know the, Laplace equation is $\frac{\partial^{2} u}{\partial \mathbf{x}^{2}}+\frac{\partial^{2} u}{\partial \mathbf{y}^{2}}=0$ this is also known as the harmonic function The solution of the function is

$$
u(x, y)=\left(C_{1} \cos \lambda x+C_{2} \sin \lambda x\right)\left(C_{3} e^{\lambda y}+C_{4} e^{-\lambda y}\right)
$$

Let

$$
A B=C D=1
$$

Using $u(x, 0)=0$

$$
\Rightarrow C_{3}=-C_{4}
$$

Using $(0, y)=0$

$$
\begin{aligned}
& \Rightarrow C_{1}=0 \\
& u(x, y)=\left(0+C_{2} \sin \lambda x\right)\left(C_{2} e^{\lambda y}-C_{3} e^{-\lambda y}\right) \\
& u(x, y)=a_{x} \sin \lambda x\left(e^{\lambda y}-e^{-\lambda y}\right)
\end{aligned}
$$

Now using $u(1, y)=0$

$$
\sin \lambda=0 \Rightarrow \lambda=\mathrm{n} \pi
$$

Hence, $\quad u(x, y)=\Sigma a_{n} \sin (n \pi n)\left[e^{n \pi y}-e^{-n \pi y}\right]$
Using $u(x, 1)=100$

$$
\Rightarrow \mathrm{a}_{1}=\frac{100}{\sin \pi \times\left[\mathrm{e}^{\pi}-\mathrm{e}^{-\pi}\right]}
$$

Using equation (iii),

$$
u(x, y)=\frac{100}{0^{\pi} 0^{-\pi}}\left(e^{\pi y}-e^{-\pi y}\right)
$$

At mid-point, i.e.,

$$
\begin{aligned}
& \mathrm{u}\left(\frac{1}{2}, \frac{1}{2}\right)=\mathrm{T}_{0} \\
& \Rightarrow \mathrm{~T}_{0}=\frac{100}{\left(\mathrm{e}^{\pi}-\mathrm{e}^{-\pi}\right)}\left(\mathrm{e}^{\pi / 2}-\mathrm{e}^{-\pi / 2}\right) \\
& =\frac{100}{\left(\mathrm{e}^{\pi / 2}+\mathrm{e}^{-\pi / 2}\right)}=\frac{100}{2 \cos \frac{\pi}{2}}=\frac{50}{2.509}=19.928=19.93^{\circ} \mathrm{C}
\end{aligned}
$$

32. An unconfined compression strength test was conducted on a cohesive soil. The test specimen failed at an axial stress of 76 kPa . The undrained cohesion (in kPa , in integer) of the soil is
$\qquad$ .
[NAT - 1 Mark]
Ans. 76
Sol. Test done on soil - UCS Axial stress $=76 \mathrm{kPa}$
For UCS test

33. The pressure in a pipe at $X$ is to be measured by an open manometer as shown in figure. Fluid A is oil with a specific gravity of 0.8 and Fluid $B$ is mercury with a specific gravity of 13.6 . The absolute pressure at $X$ is $\mathrm{kN} / \mathrm{m}^{2}$ (round off to one decimal place).
[Assume density of water as $1000 \mathrm{~kg} / \mathrm{m}^{3}$ and acceleration due to gravity as $9.81 \mathrm{~m} / \mathrm{s}^{2}$ and atmospheric pressure as $101.3 \mathrm{kN} / \mathrm{m}^{2}$ ]

[NAT - 1 Mark]
Ans. 140.5
Sol. $P_{x}-(800 \times 9.81 \times 0.75)-(13600 \times 9.81 \times 0.25)=P_{a t m}$
$P_{x}=101.3 \times 10^{3}+800 \times 9.81 \times 0.75+13600 \times 9.81 \times 0.25$
$P_{x}=140.54 \mathrm{kN} / \mathrm{m}^{2}$
34. For the elevation and temperature data given in the table, the existing lapse rate in the environment is $\qquad$ ${ }^{\circ} \mathrm{C} / 100 \mathrm{~m}$ (round off to two decimal places).

| Elevation from ground level (m) | Temperature ( ${ }^{\circ} \mathbf{C}$ ) |
| :---: | :---: |
| 5 | 14.2 |
| 325 | 16.9 |

[NAT - 1 Mark]
Ans. 0.84

## Sol.

| Elevation above ground level | Temperature |
| :---: | :---: |
| 5 m | $14.2^{\circ} \mathrm{C}$ |
| 325 m | $16.9^{\circ} \mathrm{C}$ |

$E L R=\frac{16.9-14.2}{(325-5)}$
$=0.00843^{\circ} \mathrm{C} / \mathrm{m}$
$=0.84{ }^{\circ} \mathrm{C} / 100 \mathrm{~m}$
35. If the size of the ground area is $6 \mathrm{~km} \times 3 \mathrm{~km}$ and the corresponding photo size in the aerial photograph is $30 \mathrm{~cm} \times 15 \mathrm{~cm}$, then the scale of the photograph is 1 : (in integer).
[NAT - 1 Mark]
Ans. 20,000

Sol. Ground area

$$
\begin{aligned}
& =6 \mathrm{~km} \times 3 \mathrm{~km} \\
& =30 \mathrm{~cm} \times 15 \mathrm{~cm}
\end{aligned}
$$

Photograph size
Scale

$$
\begin{aligned}
& =\sqrt{\frac{\text { photograph size }}{\text { ground size }}} \\
& =\sqrt{\frac{30 \times 15}{6 \times 3 \times\left(10^{5}\right)^{2}}} \\
& =1: 20000
\end{aligned}
$$

36. The solution of the differential equation

$$
\frac{d^{3} y}{d x^{3}}-5.5 \frac{d^{2} y}{d x^{2}}+9.5 \frac{d y}{d x}-5 y=0
$$

is expressed as $y=C_{1} e^{2.5 x}+C_{2} e^{\alpha x}$, where $C_{1}, C_{2}, C_{3}, \alpha$, and $\beta$ are constants, with $\alpha$ and $\beta$ being distinct and not equal to 2.5 . Which of the following options is correct for the values of $\alpha$ and $\beta$ ?
A. 1 and 2
B. -1 and -2
C. 2 and 3
D. -2 and -3
[MCQ - 2 Marks]
Ans. A
Sol. Auxiliary equation is,

$$
m^{3}-5.5 m^{2}+9.5 m-5=0
$$

By solving above equation, we get

$$
\text { So, } \quad \begin{aligned}
& M=2.5,1,2 \\
& m_{1} \text { and } m_{2} \text { are } 1 \text { and } 2 .
\end{aligned}
$$

37. Two vectors $\left[\begin{array}{llll}2 & 1 & 0 & 3\end{array}\right]^{\top}$ and $\left[\begin{array}{llll}1 & 0 & 1 & 2\end{array}\right]^{\top}$ belong to the null space of a $4 \times 4$ matrix of rank 2 . Which one of the following vectors also belongs to the null space?
A. $\left[\begin{array}{llll}1 & 1 & -1 & 1\end{array}\right]^{\top}$
B. $\left[\begin{array}{llll}2 & 0 & 1 & 2\end{array}\right]^{\top}$
C. $\left[\begin{array}{llll}0 & -2 & 1 & -1\end{array}\right]^{\top}$
D. $\left[\begin{array}{llll}3 & 1 & 1 & 2\end{array}\right]^{\top}$
[MCQ - 2 Marks]
Ans. A
Sol. Nullity of matrix

$$
\begin{aligned}
& =\text { No. of variables }(n)-\text { rank of } A \\
& =4-2=2
\end{aligned}
$$

and
Nullity is no. of linearly independent vectors in the null space.
After seeing the given matrix, these two vectors are already independent.
i.e., $\quad x=\left[\begin{array}{l}2 \\ 1 \\ 0 \\ 3\end{array}\right] \& y=\left[\begin{array}{l}1 \\ 0 \\ 1 \\ 2\end{array}\right]$

Any other vectors in null space

$$
z=\alpha x+\beta y
$$

Where, $\alpha, \beta$ can be any real value.

For

$$
\alpha=1 \text { and } \beta=-1
$$

$$
z=\left[\begin{array}{c}
1 \\
1 \\
-1 \\
1
\end{array}\right]=\left[\begin{array}{llll}
1 & 1 & -1 & 1
\end{array}\right]^{\top}
$$

Option A is correct.
38. Cholesky decomposition is carried out on the following square matrix [A].

$$
[A]=\left[\begin{array}{cc}
8 & -5 \\
-5 & a_{22}
\end{array}\right]
$$

Let $\mathrm{l}_{\mathrm{ij}}$ and $\mathrm{a}_{\mathrm{ij}}$ be the $(1, j)^{\text {th }}$ elements of matrices [L] and [A], respectively. If the element $\mathrm{I}_{22}$ of the decomposed lower triangular matrix [L] is 1.968, what is the value (rounded off to the nearest integer) of the element $\mathrm{a}_{22}$ ?
A. 5
B. 7
C. 9
D. 11
[MCQ - 2 Marks]
Ans. B
Sol. Cholesky decomposition

$$
A=L L^{*}
$$

Where,
$\mathrm{L}=$ Lower triangular matrix with real \& positive diagonal elements.
$L^{*}=$ Transpose of conjugate

$$
\begin{aligned}
& \mathrm{LL}^{*}=\mathrm{A} \\
& {\left[\begin{array}{ll}
\mathrm{L}_{11} & 0 \\
\mathrm{~L}_{21} & \mathrm{~L}_{22}
\end{array}\right]\left[\begin{array}{cc}
\mathrm{L}_{11} & \mathrm{~L}_{12} \\
0 & \mathrm{~L}_{22}
\end{array}\right]=\left[\begin{array}{cc}
8 & -5 \\
-5 & \mathrm{a}_{22}
\end{array}\right]}
\end{aligned}
$$

$L_{11} \& L_{22} \rightarrow$ positive and $L_{22}=1.968$ (given)
(i) $L_{11}{ }^{2}=8 \Rightarrow L_{1}=\sqrt{8}$
(ii) $L_{11} L_{21}=-5 \Rightarrow L_{21}=\frac{-5}{\sqrt{8}}$
(iii) $\mathrm{L}_{21}{ }^{2}+1.968^{2}=\mathrm{a}_{22}$
$\Rightarrow \mathrm{a}_{22}=\frac{25}{8}+1.968^{2} \cong 7$
39. In a two-dimensional stress analysis, the state of stress at a point is shown in the figure. The values of length of PQ, QR, and RP are 4, 3, and 5 units, respectively. The principal stresses are
$\qquad$ (round off to one decimal place)

A. $\sigma_{x}=26.7 \mathrm{MPa}, \sigma_{y}=172.5 \mathrm{MPa}$
B. $\sigma_{x}=54.0 \mathrm{MPa}, \sigma_{y}=128.5 \mathrm{MPa}$
C. $\sigma_{x}=67.5 \mathrm{MPa}, \sigma_{y}=213.3 \mathrm{MPa}$
D. $\sigma_{x}=16.0 \mathrm{MPa}, \sigma_{y}=138.5 \mathrm{MPa}$

Ans. C
Sol. Given,


$$
P Q=4
$$

$$
\mathrm{QR}=3 \quad \mathrm{PR}=5
$$

From fig.

$$
\begin{aligned}
& \sin \theta=\frac{3}{5}, \cos \theta \frac{4}{5} \\
& \sigma=120 \mathrm{MPa} \\
& \tau=70 \mathrm{MPa}
\end{aligned}
$$

We have,

$$
\begin{align*}
& \sigma_{\theta}=\sigma_{x x} \cos ^{2} \theta+\sigma_{y y} \sin ^{2} \theta+2 \tau_{x y} \sin \theta \cdot \cos \theta \\
& 120=\sigma_{x x}\left[\frac{4}{5}\right]^{2}+\sigma_{y y}\left(\frac{3}{5}\right)^{2}+0 \\
& 120=\frac{16}{25} \sigma_{x x}+\frac{9}{25} \times \sigma_{y y} \quad \ldots \text { (i) } \\
& \tau_{\theta}=-\left(\frac{\sigma_{x x}-\sigma_{y y}}{2}\right) \sin 2 \theta+\tau_{x y} \cos 2 \theta \\
& 70 \times 2=-\left(\sigma_{x x}-\sigma_{y y}\right) \times 2 \sin \theta \cos \theta \\
& 70 \times 2=-\left(\sigma_{x x}-\sigma_{y y}\right) \times 2 \times \frac{3}{5} \times \frac{4}{5} \\
& 12 \sigma_{x x}-12 \sigma_{y y}=-70 \times 25 \tag{ii}
\end{align*}
$$

By solving equation (i) and (ii)

$$
\begin{aligned}
& \sigma_{x x}=67.5 \mathrm{MPa} \\
& \sigma_{y y}=213.33 \mathrm{MPa}
\end{aligned}
$$

40. Two plates are connected by fillet welds of size 10 mm and subjected to tension, as shown in the figure. The thickness of each plate is 12 mm . The yield stress and the ultimate stress of steel under tension are 250 MPa and 410 MPa , respectively. The welding is done in the workshop (partial safety factor, $\gamma_{m w}=1.25$ ). As per the Limit State Method of IS 800: 2007, what is the minimum length (in mm , rounded off to the nearest higher multiple of 5 mm ) required of each weld to transmit a factored force $P$ equal to 275 kN ?

A. 100
B. 105
C. 110
D. 115

Ans. B

## Sol.



## Fillet weld:

Size

$$
\begin{aligned}
& =10 \mathrm{~mm} \\
& =90^{\circ}
\end{aligned}
$$

Fusion angle
Effective Throat thickness $=0.7 \times$ size $=0.7 \times 10=7 \mathrm{~mm}$
So,

$$
\mathrm{t}_{\mathrm{e}}=7 \mathrm{~mm}
$$

Design strength of fillet weld:

$$
P_{d w}=\frac{f_{u}}{\sqrt{3} \cdot \gamma_{m w}} \times I_{e} \times t_{e}
$$

Let's take limiting condition:

$$
\begin{aligned}
& P_{d w}=275 \times 10^{3} \mathrm{~N}=\frac{410}{\sqrt{3} \times 1.25} \times 7 \mathrm{~mm} \times l_{e} \\
& \mathrm{l}_{\mathrm{e}}=207.45 \mathrm{~mm}
\end{aligned}
$$

So, the required length on each side $=\frac{\mathrm{I}_{\mathrm{e}}}{2}=\frac{207.45}{2}$

$$
=103.72 \mathrm{~mm}
$$

Hence, nearest higher multiple of 5 mm is 105 mm .
41. In the given figure, Point $O$ indicates the stress point of a soil element at initial non-hydrostatic stress condition. For the stress path (OP), which of the following loading conditions is correct?


$$
\mathrm{p}=\frac{\sigma_{\mathrm{v}}+\sigma_{\mathrm{h}}}{2}
$$

A. $\sigma_{v}$ is increasing and $\sigma_{h}$ is constant
B. $\sigma_{v}$ is increasing and $\sigma_{h}$ is increasing
C. $\sigma_{v}$ is increasing and $\sigma_{h}$ is decreasing
D. $\sigma_{v}$ is decreasing and $\sigma_{h}$ is increasing

Ans. A
Sol.

$$
\begin{aligned}
& \mathrm{q}=\frac{\sigma_{\mathrm{v}}-\sigma_{\mathrm{h}}}{2} \\
& \mathrm{p}=\frac{\sigma_{\mathrm{v}}+\sigma_{h}}{2}
\end{aligned}
$$

When $\sigma_{v}$ increasing and $\sigma_{h}$ is constant, then the ordinates of both $x$-axis and $y$-axis will increase. It will make the stress path as given in the question. Hence option $A$ is correct.
42. The figure shows a vertical retaining wall with backfill consisting of cohesive-frictional soil and a failure plane developed due to passive earth pressure. The forces acting on the failure wedge are: P as the reaction force between the wall and the soil, R as the reaction force on the failure plane, $C$ as the cohesive force along the failure plane and $W$ as the weight of the failure wedge. Assuming that there is no adhesion between the wall and the wedge, identify the most appropriate force polygon for the wedge.

A.

B.

C.

D.


Ans. C
Sol. Force polygon for passive state:

43. A compound symmetrical open channel section as shown in the figure has a maximum of
$\qquad$ critical depth(s).

$B_{m}$ - Bottom width of main channel
$B_{f}-$ Bottom width of flood channel

$\mathrm{n}_{\mathrm{m}}$ - Manning's roughness of the main channel
$n_{f}$ - Manning's roughness of the flood channel
A. 3
B. 2
C. 1
D. 4

Ans. A
Sol. Consider the following three cases:
Case 1:
When $\mathrm{Q}=\mathrm{Q}_{1}$ and depth of flow $(\mathrm{y})<\mathrm{y}_{\mathrm{m}}$
Then, $y_{c 1}$ is the critical depth.

## Case 2:

When $Q=Q_{2}$ and depth of flow $(y)>y_{m}$
Then, $y_{c 1}, y_{c 2}$ and $y_{c 3}$ be the critical depth.

## Case 3:

When $\mathrm{Q}=\mathrm{Q} 3$
Only yc3 will exist.
So, the maximum number of critical depths will be three.

44. The critical flow condition in a channel is given by $\qquad$ .
[Note: $\alpha$ - kinetic energy correction factor; Q - discharge; $\mathrm{A}_{c}$ - cross-sectional area of flow at critical flow condition; $\mathrm{T}_{\mathrm{c}}$ - top width of flow at critical flow condition; g - acceleration due to gravity]
A. $\frac{\alpha Q^{2}}{g}=\frac{A_{c}^{3}}{T_{c}}$
B. $\frac{\alpha Q}{g}=\frac{A_{c}^{3}}{T_{c}^{2}}$
C. $\frac{\alpha Q^{2}}{g}=\frac{A_{c}^{3}}{T_{c}^{2}}$
D. $\frac{\alpha Q}{g}=\frac{A_{c}^{3}}{T_{c}}$
[MCQ - 2 Marks]
Ans. A
Sol. For critical flow condition in channel of any shape

$$
\frac{Q^{2} T_{c}}{{g A_{c}^{3}}_{3}^{3}}=1
$$

If kinetic energy factor $\alpha$ is considered.

$$
\begin{aligned}
& \frac{\alpha \mathrm{Q}^{2} \mathrm{~T}_{\mathrm{c}}}{\mathrm{gA}_{\mathrm{c}}^{3}}=1 \\
& \frac{\alpha \mathrm{Q}^{2}}{\mathrm{~g}}=\frac{\mathrm{A}_{\mathrm{c}}^{3}}{\mathrm{~T}_{\mathrm{c}}}
\end{aligned}
$$

45. Match the following air pollutants with the most appropriate adverse health effects:

| Air pollutant |  | Health effect to human and/or test animal |  |
| :---: | :---: | :---: | :---: |
| P. | Aromatic hydrocarbons | I. | Reduce the capability of the blood to <br> carry oxygen |
| Q. | Carbon monoxide | II. | Bronchitis and pulmonary emphysema |
| R | Sulfur oxides | III. | Damage of chromosomes |
| S | Ozone | IV. | Carcinogenic effect |

A. (P) - (II), (Q) - (I), (R) - (IV), (S) - (III)
B. $(P)-(I V),(Q)-(I),(R)-(I I I),(S)-(I I)$
C. $(\mathrm{P})-(\mathrm{III}),(\mathrm{Q})-(\mathrm{I}),(\mathrm{R})-(\mathrm{II}),(\mathrm{S})-(\mathrm{IV})$
D. $(\mathrm{P})-(\mathrm{IV}),(\mathrm{Q})-(\mathrm{I}),(\mathrm{R})-(\mathrm{II}),(\mathrm{S})-(\mathrm{III})$
[MCQ - 2 Marks]

## Ans. D

Sol. Aromatic hydrocarbons - Carcinogenic effect
Carbon monoxide - Reduce the capability of the blood to carry oxygen
Sulfur oxides - Bronchitis and pulmonary emphysema
Ozone - Damage of chromosomes
46. A delivery agent is at a location $R$. To deliver the order, she is instructed to travel to location $P$ along straight-line paths of $R C, C A, A B$ and $B P$ of 5 km each. The direction of each path is given in the table below as whole circle bearings. Assume that the latitude (L) and departure (D) of $R$ is $(0,0) \mathrm{km}$. What is the latitude and departure of $P$ (in km, rounded off to one decimal place)?

| Paths | $R C$ | $C A$ | $A B$ | $B P$ |
| :--- | :--- | :--- | :--- | :--- |


| Directions (in degrees) | 120 | 0 | 90 | 240 |
| :---: | :---: | :---: | :---: | :---: |

A. $L=2.5 ; D=5.0$
B. $L=0.0 ; D=5.0$
C. $L=5.0 ; D=2.5$
D. $L=0.0 ; D=0.0$
[MCQ - 2 Marks]
Ans. B
Sol. Latitude and departure of starting point, $R=(0,0) \mathrm{km}$
Latitude of location $P=$ Latitude of $R+\Sigma$ Latitude for each line

$$
\begin{aligned}
& =0+5 \cos 120^{\circ}+5 \cos 0^{\circ}+5 \cos 90^{\circ}+5 \cos 240^{\circ} \\
& =0 \mathrm{~km}
\end{aligned}
$$

Departure of location $P=$ Departure of $R+\Sigma$ Departure for each line

$$
\begin{aligned}
& =0+5 \sin 120^{\circ}+5 \sin 0^{\circ}+5 \sin 90^{\circ}+5 \sin 240^{\circ} \\
& =5 \mathrm{~km} \\
& \mathrm{~L}=0 \mathrm{~km}, \mathrm{D}=5 \mathrm{~km}
\end{aligned}
$$

Hence,
47. Which of the following statements is/are TRUE?
A. The thickness of a turbulent boundary layer on a flat plate kept parallel to the flow direction is proportional to the square root of the distance from the leading edge
B. If the streamlines and equipotential lines of a source are interchanged with each other, the resulting flow will be a sink
C. For a curved surface immersed in a stationary liquid, the vertical component of the force on the curved surface is equal to the weight of the liquid above it
D. For flow through circular pipes, the momentum correction factor for laminar flow is larger than that for turbulent flow
[MSQ - 2 Marks]
Ans. C and D
Sol.

1. Vertical component of force on curved surface immersed in a stationary liquid is equal to the weight of the liquid above the curved surface upto the free surface of the liquid. So, option A is true.
2. Momentum correction factor for flow in circular pipe

| Laminar flow | $=1.33$ |
| :--- | :--- |
| Turbulent flow | $=1.015$ |
| So, option B is true. |  |

3. Sink will form if you reverse the direction of the streamlines in the source. So, option $C$ is false.
4. Turbulent boundary layer thickness $\delta$ relation with distance $x$ from the leading edge of plate is given as

$$
\frac{\delta}{x}=\frac{0.376}{\mathrm{Re}^{1 / 5}}
$$

where,

$$
\operatorname{Re}=\frac{\rho \mathrm{VX}}{\mu}
$$

$$
\frac{\delta}{x}=\frac{0.376}{\left(\frac{\rho v x}{\mu}\right)^{1 / 5}} \Rightarrow \delta=\frac{0.376 x^{4 / 5}}{\left(\frac{\rho v}{\mu}\right)}
$$

$\therefore \delta \propto \mathrm{x}^{4 / 5}$

So, option D is false.
48. In the context of water and wastewater treatments, the correct statements are:
A. particulate matter may shield microorganisms during disinfection
B. ammonia decreases chlorine demand
C. phosphorous stimulates algal and aquatic growth
D. calcium and magnesium increase hardness and total dissolved solids
[MSQ - 2 Marks]
Ans. A, C, D
Sol.

1. Particulate matter shields microorganisms during disinfection. So, option A is correct.
2. Ammonia increases chlorine demand. So, option B is incorrect.
3. Phosphorous stimulates algal and aquatic growth. So, option $C$ is correct.

Calcium and magnesium increase hardness and total dissolved solids in water. So, option $D$ is correct.
49. Which of the following statements is/are TRUE for the aerobic composting of sewage sludge?
A. Bulking agent is added during the composting process to reduce the porosity of the solid mixture
B. Leachate can be generated during composting
C. Actinomycetes are involved in the process
D. In-vessel composting systems cannot be operated in the plug-flow mode
[MSQ - 2 Marks]
Ans. B, C

## Sol.

1. Bulking agent is added to increase the volume. So, option $A$ is incorrect.
2. Leachate can be generated during compositing. So, option B is correct.
3. Antinocytes are involved in the process. So, option $C$ is correct.

In-vessel composting, systems can be operated in plug-flow mode. So, option $D$ is incorrect.
50. The figure presents the time-space diagram for when the traffic on a highway is suddenly stopped for a certain time and then released. Which of the following statements are true?

A. Speed is higher in Region $R$ than in Region $P$
B. Volume is lower in Region $Q$ than in Region $P$
C. Volume is higher in Region $R$ than in Region $P$
D. Density is higher in Region $Q$ than in Region $R$

Ans. B, C and D

## Sol.

- Slope of distance $\mathrm{v} / \mathrm{s}$ time plot (represents speed) for region P is more than region R . So, option A is incorrect.
- Slope in region $Q$ is parallel to x-axis. It means the vehicles are not moving. So, the volume for region $Q$ is zero and density will be maximum. So, option $B$ and $D$ are correct.
Since, speed in region $P$ is more than region $R$, region $R$ will have a higher volume. So, option $C$ is correct.

51. Consider the Marshall method of mix design for bituminous mix. With the increase in bitumen content, which of the following statements is/are TRUE?
A. the Stability decreases initially and then increases
B. the Flow increases monotonically
C. the air voids (VA) increases initially and then decreases
D. the voids filled with bitumen (VFB) increases monotonically
[MSQ - 2 Marks]
Ans. B, D

## Sol.

- With increase with Bitumen content, Air voids decrease.
- With increase with Bitumen content, VFB increases.

- As Bitumen content increases, the stability increases initially then decreases.

- As Bitumen content increases, the flow will increase.


52. A 5 cm long metal rod $A B$ was initially at a uniform temperature of $\mathrm{T}_{0}{ }^{\circ} \mathrm{C}$. Thereafter, temperature at both the ends are maintained at $0^{\circ} \mathrm{C}$. Neglecting the heat transfer from the lateral surface of
the rod, the heat transfer in the rod is governed by the one-dimensional diffusion equation $\frac{\partial \mathrm{T}}{\partial \mathrm{t}}=\mathrm{D} \frac{\partial^{2} \mathrm{~T}}{\partial \mathrm{x}^{2}}$, where D is the thermal diffusivity of the metal, given as $1.0 \mathrm{~cm}^{2} / \mathrm{s}$.
The temperature distribution in the rod is obtained as

$$
\frac{\partial \mathrm{T}}{\partial \mathrm{t}}=\mathrm{D} \frac{\partial^{2} \mathrm{~T}}{\partial \mathbf{x}^{2}}
$$

where x is in cm measured from A to B with $x=0$ at $\mathrm{A}, \mathrm{t}$ is in $\mathrm{s}, \mathrm{C}_{\mathrm{n}}$ are constants in ${ }^{\circ} \mathrm{C}$, T is in ${ }^{\circ} \mathrm{C}$, and $\beta$ is in $\mathrm{s}^{-1}$.
The value of $\beta$ (in $\mathrm{s}^{-1}$, rounded off to three decimal places) is $\qquad$ -.
[NAT - 2 Marks]
Ans. 0.395
Sol. $\frac{\partial T}{\partial t}=\Delta \frac{\partial^{2} T}{\partial x^{2}} ; T(0, t)=0, T(5, t)=0, T(x, 0)=T_{0}, D=1$
Put $D=1$, it's general solution using separation of variables methods in
$T(x, t)=\left(C_{1} \operatorname{cospx}+C_{2} \sin p x\right) C_{3} e^{-p 2 t}$
Using

$$
\begin{align*}
& T(0, t)=0 \Rightarrow C_{1}=0  \tag{ii}\\
& T(5, t)=0 \Rightarrow C_{2} C_{3} \sin 5 p e^{-p 2 t}=0 \\
& \sin 5 p=0 \Rightarrow p=\frac{n \pi}{5}, n \in I
\end{align*}
$$

Using
Or

Hence by (2),

$$
T(x, t)=b_{n} \sin \left(\frac{n \pi x}{5}\right) \cdot e^{\frac{-n^{2} \pi^{2} t}{25}} \quad \text { Where } b_{n}=C_{2} C_{3}
$$

Hence most general solution is

$$
\begin{equation*}
T(x, t)=\sum_{n=1}^{\infty} b_{n} \sin \left(\frac{n \pi x}{5}\right) \cdot e^{\frac{-n^{2} \pi^{2} t}{25}} \tag{iii}
\end{equation*}
$$

Now using $T(x, 0)=T 0$

$$
\Rightarrow T_{0}=\sum_{n=1}^{\infty} b_{n} \sin \left(\frac{n \pi x}{5}\right)
$$

Which is half range fourier sine series for $T_{0}$
Hence,

By (3)

$$
T(x, t)=\sum_{n=1,3,5} C_{n} \sin \left(\frac{n \pi x}{5}\right) e^{-\beta n^{2} t}
$$

$$
\Rightarrow \quad \mathrm{C}_{\mathrm{n}}=\frac{4 \mathrm{~T}_{0}}{\mathrm{n} \pi} \text { and } \beta=\frac{\pi^{2}}{25}=0.3947 \approx 0.395
$$

53. A beam is subjected to a system of coplanar forces as shown in the figure. The magnitude of vertical reaction at Support P is N (round off to one decimal place).

$$
\begin{align*}
& b_{n}=\frac{2}{5} \int_{0}^{5} T_{0} \sin \left(\frac{n \pi x}{5}\right) d x=\left\{\begin{array}{cc}
0 & n \text { even } \\
\frac{4 T_{0}}{n \pi} & n \text { odd }
\end{array}\right. \\
& T(x, t)=\sum_{n=o d d} \frac{4 T_{0}}{n \pi} \sin \left(\frac{n \pi x}{5}\right) e^{\frac{-n^{2} \pi^{2} t}{25}} \tag{iv}
\end{align*}
$$


[NAT - 2 Marks]
Ans. 197.06
Sol. Let vertical reaction at support $P=V_{p}$


Sum of vertical force $\Sigma \mathrm{V}=0$

$$
\begin{align*}
& V_{P}+V_{Q}=500 \sin 60^{\circ}-200 \mathrm{~N} \\
& V_{P}+V_{Q}=2330.01 \mathrm{~N}
\end{align*}
$$

Moment about point $\mathrm{Q}, \Sigma \mathrm{M}_{\mathrm{Q}}=0$

$$
\begin{aligned}
& V_{P} \times 6+200 \times 2.5-500 \sin 60^{\circ} \times 4+50=0 \\
& V_{P}=197.06 \mathrm{~N}
\end{aligned}
$$

54. For the frame shown in the figure (not to scale), all members ( $A B, B C, C D, G B$, and $C H$ ) have the same length, $L$ and flexural rigidity, $E I$. The joints at B and C are rigid joints, and the supports $A$ and $D$ are fixed supports. Beams $G B$ and $C H$ carry uniformly distributed loads of $w$ per unit length. The magnitude of the moment reaction at $A$ is $w L^{2} / k$. What is the value of $k$ (in integer)?

[NAT - 2 Marks]
Ans. 6
Sol.


Stiffness of $B C=\frac{2 E I}{L}$
(Since, the beam is bending in a symmetrical mode)
Stiffness of $B A=\frac{4 E I}{L}$

$$
\begin{aligned}
& \text { D.F. for } B A=\frac{\frac{4 E I}{L}}{\frac{4 E I}{L}+\frac{2 E I}{L}}=\frac{2}{3} \\
& M_{B A}=\frac{w L^{2}}{2} \times \frac{2}{3}=\frac{2 w L^{2}}{6}
\end{aligned}
$$

Carry over moment at $A, M_{A B}=\frac{1}{2} \times \frac{2 w L^{2}}{6}$

$$
\begin{aligned}
& =\frac{w L^{2}}{6} \\
& \Rightarrow k=6
\end{aligned}
$$

55. Consider the singly reinforced section of a cantilever concrete beam under bending, as shown in the figure (M25 grade concrete, Fe415 grade steel). The stress block parameters for the section at ultimate limit state, as per IS 456: 2000 notations, are given. The ultimate moment of resistance for the section by the Limit State Method is $\qquad$ kN.m (round off to one decimal place).
[Note: Here, $A_{s}$ is the total area of tension steel bars, $b$ is the width of the section, $d$ is the effective depth of the bars, $f_{c k}$ is the characteristic compressive cube strength of concrete, $f_{y}$ is the yield stress of steel, and $x_{u}$ is the depth of neutral axis.]

[NAT - 2 Marks]
Ans. 300.9
Sol.
$B=300 \mathrm{~mm}$
```
\(A_{\text {st }}=3-28 \mathrm{~mm}\)
Effective cover
    \(=45 \mathrm{~mm}\)
    \(D=600 \mathrm{~mm}\)
    \(\mathrm{d}=600-45=555 \mathrm{~mm}\)
    \(\mathrm{Xu}_{\mathrm{u} \text { lim }}=\mathrm{kd}\) \{for Fe 415, \(\mathrm{k}=0.48\) \}
    \(=0.48 \mathrm{~d}\)
    \(=0.48 \times 555\)
    \(=266.4 \mathrm{~mm}\)
    \(\mathrm{C}=\mathrm{T}\)
    \(0.36 f_{c k} B x_{u}=0.87 f_{y} A_{\text {st }}\).
    \(0.36 \times 25 \times 300 \times x_{u}=0.87 \times 415 \times \frac{\pi}{4} \times 28^{2} \times 3\)
    \(X_{u}=247 \mathrm{~mm}\)
Now,
    \(X_{u}<X_{u l i m}\)
```

So, it's an under-reinforced section.

$$
\begin{aligned}
& M O R=0.36 f_{c k} B x_{u}\left(d-0.42 x_{u}\right) \\
& =0.36 \times 25 \times 300 \times 247[555-(0.42 \times 247)] \\
& =300.9 \mathrm{kNm}
\end{aligned}
$$

56. A 2 D thin plate with modulus of elasticity, $E=1.0 \mathrm{~N} / \mathrm{m}^{2}$, and Poisson's ratio, $\mu=0.5$, is in plane stress condition. The displacement field in the plate is given by $u=C x^{2} y$ and $v=0$ and $v=0$, where $u$ and $v$ are displacements (in $m$ ) along the $X$ and $Y$ directions, respectively, and $C$ is a constant (in $\mathrm{m}^{-2}$ ). The distances $x$ and $y$ along $X$ and $Y$, respectively, are in $m$. The stress in the $X$ direction is $\sigma_{x x}=40 x y \mathrm{~N} / \mathrm{m}^{2}$, and the shear stress is $\tau_{x y}=\alpha x^{2} N / m^{2}$. What is the value of $\alpha$ (in $\mathrm{N} / \mathrm{m}^{4}$, in integer)? $\qquad$ .
[NAT - 2 Marks]
Ans. 7
Sol. We have given.

$$
\mathrm{E}=1 \mathrm{~N} / \mathrm{m}^{2}, \mu=0.5, \sigma_{x x}=40 x y \mathrm{~N} / \mathrm{m}^{2} \text { and } \tau_{x y}=\alpha \mathrm{x}^{2} \mathrm{~N} / \mathrm{m}^{2}
$$

The stress strain variation is assumed to be linear.
Strain in X - direction

$$
\epsilon_{x}=\frac{\sigma_{x}}{E}-\frac{\mu \sigma_{x}}{E}
$$

Strain in Y - direction

$$
\begin{aligned}
& \epsilon_{y}=\frac{\sigma_{y}}{E}-\frac{\mu \sigma_{x}}{E} \\
& \gamma_{x y}=\frac{\tau_{x y}}{G}
\end{aligned}
$$

Also,

$$
G=\frac{E}{2(1+\mu)}
$$

$$
\epsilon_{x}+\mu \epsilon_{y}=\frac{\sigma_{x}}{E}-\frac{\mu \sigma_{y}}{E}+\frac{\mu \sigma_{y}}{E}-\frac{\mu^{2} \sigma_{x}}{E}
$$

$$
\epsilon_{\mathrm{x}}+\mu \epsilon_{\mathrm{y}}=\frac{\sigma_{\mathrm{x}}}{\mathrm{E}}\left(1-\mu^{2}\right)
$$

$$
\sigma_{x}=\frac{E}{1-\mu^{2}}\left[\epsilon_{x}+\mu \epsilon_{y}\right]
$$

$$
\sigma_{\mathrm{x}}=\frac{\mathrm{E}}{1-\mu^{2}}\left[\frac{\partial \mathbf{u}}{\partial \mathrm{x}}+\mu \frac{\partial \mathbf{v}}{\partial \mathbf{y}}\right]
$$

We have

$$
\begin{align*}
& u=C x^{2} y \\
& \frac{\partial u}{\partial x}=2 C x y \\
& \sigma_{x}=\frac{2 E C x y}{1-\mu^{2}} \\
& \Rightarrow \frac{2 E C x y}{1-\mu^{2}}=40 x y \\
& \frac{2 E C}{1-\mu^{2}}=40 \tag{i}
\end{align*}
$$

And

$$
\begin{aligned}
& \gamma_{x y}=\frac{\tau_{x y}}{G} \\
& G \gamma_{x y}=\tau_{x y}
\end{aligned}
$$

Shear strain,

$$
\begin{aligned}
& \gamma_{x y}=\frac{\partial u}{\partial y}+\frac{\partial v}{\partial x}=0+C x^{2} \\
& \frac{E}{2(1+\mu)}\left[\frac{\partial u}{\partial y}+\frac{\partial v}{\partial x}\right]=T_{x y} \\
& \frac{E}{2(1+\mu)}\left[C x^{2}+0\right]=a x^{2} \\
& a=\frac{C E}{2(1+\mu)}
\end{aligned}
$$

Put the value of CE from equation (i)

$$
\begin{aligned}
& a=\frac{40\left(1-\mu^{2}\right)}{2 E} \frac{E}{2(1+\mu)} \\
& a=10(1+\mu)=10(1-0.5)=5 \\
& a=5
\end{aligned}
$$

57. An idealised frame supports a load as shown in the figure. The horizontal component of the force transferred from the horizontal member $P Q$ to the vertical member RS at $P$ is $N$ (round off to one decimal place).


Ans. 18
Sol.

Horizontal component is

$\Sigma M_{P}=0$
$-10 \times(1.2+0.6)+F_{\mathrm{TU}} \sin \theta \times 1.2=0$
$1.2 \times \mathrm{F}_{\mathrm{TU}} \times \frac{1}{1.5620}=10(1.8)$

$$
\mathrm{F}_{\mathrm{TU}}=23.43 \mathrm{~N}
$$

58. A square footing is to be designed to carry a column load of 500 kN which is resting on a soil stratum having the following average properties: bulk unit weight $=19 \mathrm{kN} / \mathrm{m}^{3}$; angle of internal friction $=0^{\circ}$ and cohesion $=25 \mathrm{kPa}$. Considering the depth of the footing as 1 m and adopting Meyerhof's bearing capacity theory with a factor of safety of 3 , the width of the footing (in m ) is
$\qquad$ (round off to one decimal place)
[Assume the applicable shape and depth factor values as unity; ground water level at greater depth.]
[NAT - 2 Marks]
Ans. 3 to 3.4
Sol. As per Meyerhof's method

$$
\begin{aligned}
& \mathrm{q}_{\mathrm{u}}=\mathrm{CN} \mathrm{~N}_{\mathrm{c}} \mathrm{~d}_{\mathrm{c}} \mathrm{~s}_{\mathrm{c}} \mathrm{i}_{\mathrm{c}}+\gamma \mathrm{D}_{\mathrm{f}} \mathrm{~N}_{\mathrm{q}} \mathrm{~d}_{\mathrm{q}} \mathrm{~S}_{\mathrm{q}} \mathrm{i}_{\mathrm{q}}+0.5 \mathrm{~B} \gamma \mathrm{~N}_{\gamma} \mathrm{d}_{\gamma} \mathrm{s}_{\gamma} \mathrm{i}_{\gamma} \\
& \mathrm{N}_{\mathrm{q}}=1, \mathrm{~N}_{\gamma}=0, \mathrm{~N}_{\mathrm{c}}=5.14 \\
& \mathrm{C}=25 \mathrm{kPa}, \phi=0^{\circ}, \gamma=19 \mathrm{kN}
\end{aligned}
$$

Putting the value in equation

Area

$$
\begin{aligned}
& q_{u}=147.5 \mathrm{kN} / \mathrm{m}^{2} \\
& \mathrm{q}_{\mathrm{nu}}=\mathrm{q}_{\mathrm{u}}-\gamma \mathrm{D}_{\mathrm{f}} \\
& \mathrm{q}_{\mathrm{nu}}=147.5-19 \times 1=128.5 \mathrm{kN} / \mathrm{m}^{2} \\
& =\frac{\text { Load } \times F O S}{\mathrm{q}_{\mathrm{nu}}}=\frac{500 \times 3}{128.5}=11.67 \mathrm{~m}^{2}
\end{aligned}
$$

Since it's a square footing
Area $=(\text { width })^{2}$
Width $\quad=\sqrt{11.67}=3.4 \mathrm{~m}$
59. A circular pile of diameter 0.6 m and length 8 m was constructed in a cohesive soil stratum having the following properties: bulk unit weight $=19 \mathrm{kN} / \mathrm{m}^{3}$; angle of internal friction $=0^{\circ}$ and cohesion $=25 \mathrm{kPa}$.

The allowable load the pile can carry with a factor of safety of 3 is $\qquad$ kN (round off to one decimal place).
[Adopt: Adhesion factor, $\alpha=1.0$ and Bearing capacity factor, $N_{c}=9.0$ ]
[NAT - 2 Marks]
Ans. 146.5 to 146.9
Sol.

$$
\begin{aligned}
& Q_{u p}=\mathrm{q}_{s} A_{s}+\mathrm{q}_{\mathrm{b}} A_{b} \\
& \text { Qup }_{\mathrm{up}}=\bar{\alpha} \overline{\mathrm{C}}(\pi \mathrm{dL})+\mathrm{CN}_{\mathrm{c}} \frac{\pi}{4} \mathrm{~d}^{2} \\
& \text { Qup }=(1 \times 25 \times \pi \times 0.6 \times 8)+\left(25 \times 9 \times \frac{\pi}{4} \times 0.6^{2}\right) \\
& \text { Qup }=440.60 \mathrm{kN} \\
& \text { Qallowable }=\mathrm{Qup}_{\text {up }} / F O S=440.60 / 3=146.87 \mathrm{kN}
\end{aligned}
$$

60. For the flow setup shown in the figure (not to scale), the hydraulic conductivities of the two soil samples, Soil 1 and Soil 2, are $10 \mathrm{~mm} / \mathrm{s}$ and $1 \mathrm{~mm} / \mathrm{s}$, respectively. Assume the unit weight of water as $10 \mathrm{kN} / \mathrm{m}^{3}$ and ignore the velocity head. At steady state, what is the total head (in m , rounded off to two decimal places) at any point located at the junction of the two samples?

[NAT - 2 Marks]
Ans. 4.54
Sol.


Note: Unless mentioned downstream end is taken as datum.
Pressure at

$$
\begin{aligned}
& A=10 \mathrm{kPa} \\
& Y \times H=10
\end{aligned}
$$

Since,

$$
\begin{aligned}
& Y=10 \mathrm{kN} / \mathrm{m}^{3} \\
& \Rightarrow \mathrm{H}=1 \mathrm{~m}
\end{aligned}
$$

PH at $\mathrm{A}=1+1=2 \mathrm{~m}$

|  | V.H | D.H | P.H | T.H |
| :---: | :---: | :---: | :---: | :---: |
| A | 0 | 3 | 2 | 5 |
| C | 0 | 0 | 0 | 0 |

$$
H_{L}=5-0=5 \mathrm{~m}
$$

As flow is perpendicular to bedding plane $: \mathrm{Q}=$ constant

$$
\begin{aligned}
& \mathrm{K}_{\text {total }} \times\left(\frac{\mathrm{H}_{\mathrm{L}}}{\mathrm{~L}}\right)_{\text {Total }} \mathrm{A}=\frac{\mathrm{k}_{1} \mathrm{~h}_{\mathrm{L} 1}}{\mathrm{~L}_{1}} \mathrm{~A} \\
& \frac{1+1}{\frac{1}{10}+\frac{1}{1}} \times \frac{5}{2} \times \mathrm{A}=10 \times \frac{\mathrm{h}_{\mathrm{L} 1}}{1} \times \mathrm{A} \\
& \mathrm{~h}_{\mathrm{L} 1}=0.4545 \\
& \left(\mathrm{~T}_{\mathrm{H}}\right)_{\mathrm{B}}=5-1 \times .4545=4.54 \mathrm{~m}
\end{aligned}
$$

61. A consolidated drained (CD) triaxial test was carried out on a sand sample with the known effective shear strength parameters, $\mathrm{c}^{\prime}=0$ and $\phi^{\prime}=30^{\circ}$. In the test, prior to the failure, when the sample was undergoing axial compression under constant cell pressure, the drainage valve was accidentally closed. At the failure, 360 kPa deviatoric stress was recorded along with 70 kPa pore water pressure. If the test is repeated without such error, and no back pressure is applied in either of the tests, what is the deviatoric stress (in kPa , in integer) at the failure? $\qquad$
[NAT - 2 Marks]
Ans. 500
Sol.

$$
\begin{aligned}
& \bar{\sigma}_{1}=\bar{\sigma}_{3} \tan ^{2}\left(45+\frac{\phi}{2}\right)+2 c^{\prime} \tan \left(45+\frac{\phi}{2}\right) \\
& \because \bar{\sigma}_{3}=\sigma_{3}-70 \\
& \bar{\sigma}_{1}=\sigma_{1}-70=\sigma_{3}+\sigma_{d}-70=\left(\sigma_{3}+360-70\right) \\
& \Rightarrow\left(\sigma_{3}+360-70\right)=\left(\sigma_{3}-70\right) \tan ^{2}(45+30 / 2) \\
& \Rightarrow \sigma_{3}=250 \mathrm{kPa} \\
& \sigma_{1}=\sigma_{3} \tan ^{2}(45+\phi / 2) \\
& \Rightarrow\left(\sigma_{3}+\sigma_{d}\right)=\sigma_{3} \tan ^{2}(45+30 / 2) \\
& \Rightarrow\left(250+\sigma_{d}\right)=250 \times 3 \\
& \Rightarrow \sigma_{d}=500 \mathrm{kPa}
\end{aligned}
$$

62. A catchment may be idealized as a circle of radius 30 km . There are five rain gauges, one at the center of the catchment and four on the boundary (equi-spaced), as shown in the figure (not to scale).
The annual rainfall recorded at these gauges in a particular year are given below.

| Gauge | $\mathrm{G}_{1}$ | $\mathrm{G}_{2}$ | $\mathrm{G}_{3}$ | $\mathrm{G}_{4}$ | $\mathrm{G}_{5}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rainfall (mm) | 910 | 930 | 925 | 895 | 905 |

Using the Thiessen polygon method, what is the average rainfall (in mm, rounded off to two decimal places) over the catchment in that year? $\qquad$

[NAT - 2 Marks]
Ans. 912.55

## Sol.


$A_{1}=30 \times 30=900 \mathrm{~km}^{2}$

$$
A_{2}=A_{3}=A_{4}=A_{5}=\left(\frac{\pi \times 30^{2}-900}{4}\right)
$$

$$
=481.85 \mathrm{~km}^{2}
$$

$$
\text { Pavg }=\left(\frac{P_{1} A_{1}+P_{2} A_{2}+P_{3} A_{3}+P_{4} P_{4}+P_{5} P_{5}}{A_{1}+A_{2}+A_{4}+A_{5}}\right)
$$

$900 \times 910 \times 930 \times 481.85+925 \times 481.85+895+481.85+905 \times 481.89$

$$
900+4 \times 481.85
$$

$$
\mathrm{P}_{\mathrm{avg}}=912.55 \mathrm{~mm}
$$

63. The cross-section of a small river is sub-divided into seven segments of width 1.5 m each. The average depth, and velocity at different depths were measured during a field campaign at the middle of each segment width. The discharge computed by the velocity area method for the given data is $\qquad$ $\mathrm{m}^{3} / \mathrm{s}$ (round off to one decimal place).

| Segment | Average depth (D) (m) | Velocity (m/s) at different depths |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathbf{0 . 2 D}$ | $\mathbf{0 . 6 D}$ | $\mathbf{0 . 8 D}$ |
| 1 | 0.40 | - | 0.40 | - |
| 2 | 0.70 | 0.76 | - | 0.70 |
| 3 | 1.20 | 1.19 | - | 1.13 |


| 4 | 1.40 | 1.25 | - | 1.10 |
| :---: | :---: | :---: | :---: | :---: |
| 5 | 1.10 | 1.13 | - | 1.09 |
| 6 | 0.80 | 0.69 | - | 0.65 |
| 7 | 0.45 | - | 0.42 | - |

[NAT - 2 Marks]
Ans. 8.4 to 8.6

## Sol.

| Segment | Avg. Depth <br> (Y) | Avg. width(W) | V0.2 | V0.6 | $\mathrm{V}_{0.8}$ | $Q=\mathbf{Y} \times \mathbf{W} \times$ Mean <br> Velocity( $\mathrm{m}^{3} / \mathrm{s}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (i) | (ii) | (iii) | (iv) | (v) | (vi) | (vii) |
| 1 | 0.40 | 1.6875 | - | 0.40 |  | $0.4 \times 1.6875 \times .4=0.27$ |
| 2 | 0.70 | 1.5 | 0.76 | - | 0.70 | $\begin{aligned} 0.70 \times 1.5 & \times\left[\frac{0.76+0.70}{2}\right] \\ & =0.767 \end{aligned}$ |
| 3 | 1.20 |  | 1.19 | - | 1.13 | $\begin{gathered} 1.20 \times 1.5 \times\left[\frac{1.19+1.13}{2}\right] \\ =2.088 \end{gathered}$ |
| 4 | $1.40$ | 1.5 | 1.25 | - | 1.10 | $\begin{gathered} 1.40 \times 1.5 \times\left[\frac{1.25+1.10}{2}\right] \\ =2.467 \end{gathered}$ |
| 5 | $1.10$ | 1.5 | 1.13 | - | 1.09 | $\begin{gathered} 1.10 \times 1.5 \times\left[\frac{1.13+1.09}{2}\right] \\ =1.8315 \end{gathered}$ |
| 6 | $0.80$ | 1.5 | 0.69 | - | 0.65 | $\begin{aligned} 0.80 \times 1.5 & \times\left[\frac{0.09+0.05}{2}\right] \\ & =0.804 \end{aligned}$ |
| 7 | 0.45 | 1.6876 |  | 0.42 |  | $0.45 \times 1.6875 \times 0.42=0.319$ |
|  |  |  |  |  |  | Total Discharge $=8.546$ |

Average width calculation column (iii)

$$
\begin{aligned}
& \left(\mathrm{W}_{2}\right)_{\text {avg. }}=\frac{1.5}{2}+\frac{1.5}{2}=1.5 \\
& \mathrm{~W}_{2}=\mathrm{W}_{3}=\mathrm{W}_{4}=\mathrm{W}_{5}=\mathrm{W}_{6}=1.5
\end{aligned}
$$

$$
W_{\text {avg. }}=\frac{W_{1}+\frac{W_{2}}{2}}{2 W_{1}}=\frac{1.5+\left(\frac{1.5}{2}\right)^{2}}{2 \times 1.5}=1.6875
$$

## Discharge calculation, column (vii)

Discharge $=$ Average depth $\times$ average width $\times$ mean velocity
64. The theoretical aerobic oxidation of biomass $\left(\mathrm{C}_{5} \mathrm{H}_{7} \mathrm{O}_{2} \mathrm{~N}\right)$ is given below:

$$
\mathrm{C}_{5} \mathrm{H}_{7} \mathrm{O}_{2} \mathrm{~N}+5 \mathrm{O}_{2} \rightarrow 5 \mathrm{CO}_{2}+\mathrm{NH}_{3}+2 \mathrm{H}_{2} \mathrm{O}
$$

The biochemical oxidation of biomass is assumed as a first-order reaction with a rate constant of $0.23 / \mathrm{d}$ at $20^{\circ} \mathrm{C}$ (logarithm to base e). Neglecting the second-stage oxygen demand from its biochemical oxidation, the ratio of BOD5 at $20^{\circ} \mathrm{C}$ to total organic carbon (TOC) of biomass is (round off to two decimal places).
[Consider the atomic weights of $\mathrm{C}, \mathrm{H}, \mathrm{O}$ and N as $12 \mathrm{~g} / \mathrm{mol}, 1 \mathrm{~g} / \mathrm{mol}, 16 \mathrm{~g} / \mathrm{mol}$ and $14 \mathrm{~g} / \mathrm{mol}$, respectively]

Ans. 1.82
Sol. $\mathrm{C}_{5} \mathrm{H}_{7} \mathrm{O}_{2} \mathrm{~N}=5 \times(12)+7 \times(1)+2 \times(16)+14=113 \mathrm{~g}$ 113 gm of $\mathrm{C}_{5} \mathrm{H}_{7} \mathrm{O}_{2} \mathrm{~N} \rightarrow 5 \times 12 \mathrm{gm}$ carbon
1 mole of $\mathrm{C}_{5} \mathrm{H}_{7} \mathrm{O}_{2} \mathrm{~N} \rightarrow \frac{5 \times 12}{113}=0.53 \mathrm{gm}$ carbon
$\mathrm{BOD}_{5}$ at $20^{\circ} \mathrm{C}=\mathrm{BOD}_{\mathrm{u}}\left[1-\mathrm{e}^{-\mathrm{Kd} \times \mathrm{t}}\right]$
$=B O D_{u}\left(1-\mathrm{e}^{-0.23 \times 5}\right)$
$113 \mathrm{gm} \mathrm{C} \mathrm{C}_{5} \mathrm{O}_{2} \mathrm{~N}$ required $5 \times 32 \mathrm{gm}$ of $\mathrm{O}_{2}$
So, $1 \mathrm{gm} \mathrm{C} \mathrm{C}_{5} \mathrm{H}_{7} \mathrm{O}_{2} \mathrm{~N}$ requires.
$\frac{5 \times 32}{113}=1.415 \mathrm{gm}$ of $\mathrm{O}_{2}$
$\mathrm{BOD}_{\mathrm{u}}=1.4159\left(1-\mathrm{e}^{-0.23 \times 5}\right)=0.967 \mathrm{~g} / \mathrm{l}$
$\frac{\mathrm{BOD}_{5,20^{\circ} \mathrm{C}}}{\mathrm{TOC}}=\frac{0.967}{0.53}=1.82$
65. A system of seven river segments is shown in the schematic diagram. The Ri's, $\mathrm{Q}_{\mathrm{i}}$ 's, and $\mathrm{C}_{\mathrm{i}}$ 's ( $i=1$ to 7 ) are the river segments, their corresponding flow rates, and concentrations of a conservative pollutant, respectively. Assume complete mixing at the intersections, no additional water loss or gain in the system, and steady state condition. Given: $\mathrm{Q}_{1}=5 \mathrm{~m}^{3} / \mathrm{s} ; \mathrm{Q}_{2}=15 \mathrm{~m}^{3} / \mathrm{s}$; $\mathrm{Q}_{4}=3 \mathrm{~m}^{3} / \mathrm{s} ; \mathrm{Q} 6=8 \mathrm{~m}^{3} / \mathrm{s} ; \mathrm{C}_{1}=8 \mathrm{~kg} / \mathrm{m}^{3} ; \mathrm{C}_{2}=12 \mathrm{~kg} / \mathrm{m}^{3} ; \mathrm{C}_{6}=10 \mathrm{~kg} / \mathrm{m}^{3}$. What is the steady state concentration (in $\mathrm{kg} / \mathrm{m}^{3}$, rounded off to two decimal place) of the pollutant in the river segment 7 ? $\qquad$

[NAT - 2 Marks]
Ans. 10.68
Sol.

$$
\begin{aligned}
& \mathrm{Q}_{1}+\mathrm{Q}_{2}=\mathrm{Q}_{3} \\
& \mathrm{Q}_{3}=5+15=20 \mathrm{~m}^{3} / \mathrm{s} \\
& \mathrm{Q}_{3}-\mathrm{Q}_{4}=\mathrm{Q}_{5}
\end{aligned}
$$

$\mathrm{Q}_{5}=20-3=17 \mathrm{~m}^{3} / \mathrm{s}$
$\mathrm{Q}_{5}+\mathrm{Q}_{6}=\mathrm{Q}_{7}$
$\mathrm{Q}_{7}=17+8=25 \mathrm{~m}^{3} / \mathrm{s}$
$\mathrm{C}_{3}=\frac{\mathrm{C}_{1} \mathrm{Q}_{1}+\mathrm{C}_{2} \mathrm{Q}_{2}}{\mathrm{Q}_{1}+\mathrm{Q}_{2}}$
$=\frac{(8 \times 5)+(12 \times 15)}{5+15}=11 \mathrm{~kg} / \mathrm{m}^{3}$
$\mathrm{C}_{3}=\mathrm{C}_{5}=11 \mathrm{~kg} / \mathrm{m}^{3}$
$C_{7}=\left(\frac{C_{5} Q_{5}+C_{6} Q_{6}}{Q_{5}+Q_{6}}\right)=\frac{(11 \times 17+10 \times 8)}{(17+8)}$
$=10.68 \mathrm{~kg} / \mathrm{m}^{3}$

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