

# AE/JE Foundation

Mechanical Engineering

Strength of Materials

▶ Top 100  
Most Expected Questions



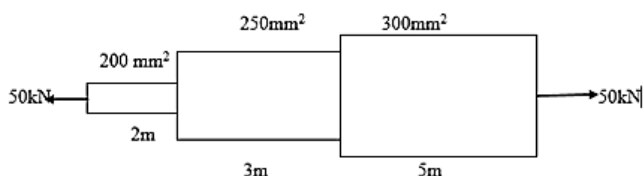


6. What is the hoop stress generated in a thin spherical shell of diameter 120mm and thickness 5mm filled with oil at a pressure of 5MPa?
- A. 10MPa    B. 20MPa  
C. 30MPa    D. 40MPa

Ans. C

Sol. Hoop stress in sphere =  $pd/4t$   
 $= (5 \times 120) / (4 \times 5)$   
 $= 30\text{MPa}$

7. Find the total extension in the stepped bar with an axial tensile load of 50 kN and having varying length of 2m, 3m, 5m and area of  $200\text{mm}^2$ ,  $250\text{mm}^2$  and  $300\text{mm}^2$  as shown in given figure.  $E = 2 \times 10^5 \text{N/mm}^2$ .



- A. 9.67mm    B. 9.82mm  
C. 9.78mm    D. 10.67mm

Ans. A

Sol. Total change in length in the stepped bar:

$$\Delta L = \frac{PL_1}{A_1E} + \frac{PL_2}{A_2E} + \frac{PL_3}{A_3E}$$

$$\Delta L = \frac{P}{E} \left( \frac{L_1}{A_1} + \frac{L_2}{A_2} + \frac{L_3}{A_3} \right)$$

$$\Delta L = \frac{50 \times 10^3}{2 \times 10^5} \left( \frac{2000}{200} + \frac{3000}{250} + \frac{5000}{300} \right)$$

$$\Delta L = 9.67\text{mm}$$

8. A cantilever beam A with rectangular cross section is subjected to a concentrated load at its free end. If width and depth of another cantilever beam B are twice those of beam A, then the deflection at free end of the beam B compared to that of A will be:
- A. 6.25 %    B. 14 %  
C. 23.6 %    D. 28 %

Ans. A

Sol.

Deflection for a point load at the free end in the cantilever beam is,  $\delta_A = \frac{WL^3}{3EI}$

Where  $I_A = \frac{bd^3}{12}$  for rectangular section

$$I_B = \frac{(2b)(2d)^3}{12}$$

$$I_B = 16 I_A$$

Deflection is inversely proportional to moment of inertia. By doubling the width and depth, moment of inertia will become 16 times that of original. So deflection

$$\delta_B = \frac{1}{16} \delta_A = 6.25\% \delta_A$$

9. A cantilever beam of span  $L$  is subjected to a moment  $M$  at its mid span. The strain energy stored in the beam due to the loading is

A.  $\frac{M^2 L}{EI}$

B.  $\frac{M^2 L}{2EI}$

C.  $\frac{M^2 L}{4EI}$

D.  $\frac{M^2 L}{8EI}$

Ans. C

Sol.

$$\text{Strain energy stored in the bar due to moment at mid span} = \int_0^{L/2} \frac{M^2 dx}{2EI} = \frac{M^2 L}{4EI}$$

10. What is the volumetric strain in the thin cylinder subjected to internal pressure having hoop stress of 200 MPa, modulus of elasticity,  $E=200$  GPa and poisons ratio=0.25?

A.  $2 \times 10^{-2}$

B.  $2 \times 10^{-3}$

C.  $1 \times 10^{-3}$

D.  $1 \times 10^{-2}$

Ans. B

Sol. Given,

Hoop stress = 200 MPa,

modulus of elasticity,  $E=200$  GPa

poisson's ratio=0.25

$$\sigma_H = \frac{Pd}{2t} = 200 \text{MPa}$$

$$\epsilon_v = \frac{Pd}{4tE} (5 - 4\mu) = \frac{1}{2E} \times \frac{Pd}{2t} (5 - 4 \times 0.25)$$

$$\epsilon_v = \frac{1}{2 \times 200 \times 10^3} \times 200 \times 4$$

$$\epsilon_v = 2 \times 10^{-3}$$

11. For a thin spherical shell subjected to internal pressure, the ratio of volumetric strain to diametrical strain is \_\_\_\_\_.

A. 5 : 4

B. 3 : 2

C. 2 : 1

D. 3 : 1

Ans. D

Sol. Volume of sphere

$$V = \frac{\pi}{6} D^3$$

Taking differential on both side

$$\delta V = 3 \times \frac{\pi}{6} \times d^2 \delta d$$

$$\delta V = 3 \times \frac{\pi}{6} d^3 \times \frac{\delta d}{d}$$

$$\delta V = 3 \times V \times \frac{\delta d}{d}$$

$$\frac{\delta V}{V} = 3 \frac{\delta d}{d}$$

So, option D is correct.

12. What is the value of bending stress for a bar of diameter 75 mm for moment of  $6.75 \times 10^3$  Nm ?

- A. 162.92 Mpa
- B. 325.95 MPa
- C. 625.95 Mpa
- D. 651.90 MPa

Ans. A

Sol. **Solution:**

We know that

$$\frac{M}{I} = \frac{\sigma_b}{y}$$

$$\therefore \sigma_b = \frac{6.75 \times 10^6 \times 64}{\pi (75)^4} \times \frac{75}{2}$$

$$\sigma_b = 162.92 \text{ MPa}$$

13. Resilience of a material is important, when it is subjected to \_\_\_\_\_.

- A. combined loading
- B. fatigue
- C. thermal stresses
- D. shock loading

Ans. D

Sol.

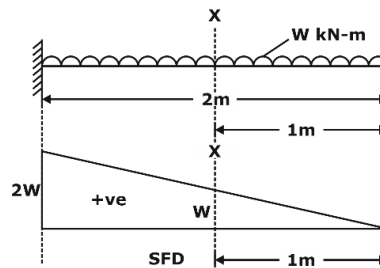
- Resilience is defined as the maximum energy that can be absorbed by a material without creating a permanent distortion.
- Resilience is important property for shock applications such as springs.

14. A uniformly distributed load  $w$  (in KN/m) is acting over the entire length of a 2 m long cantilever beam. If the shear force at the midpoint of cantilever is 5 KN. What is the value of  $w$  \_\_\_\_\_?

- A. 2
- B. 3
- C. 4
- D. 5

Ans. D

Sol. Shear force at any cross-section X-X of cantilever from free end:



$$(S.F)_{x-x} = wx$$

The value is given:  $w = 5 \text{ kN}$  at  $x = 1\text{m}$

Thus,  $w \times 1 = 5$

$w = 5 \text{ kN}$

15. When both ends of a column are fixed, the crippling load is  $F$ . If one end of the column is made free, the value of crippling load will be changed to \_\_\_\_\_.

- A.  $F/4$
- B.  $F/2$
- C.  $F/16$
- D.  $4F$

Ans. C

Sol. When both end fixed then effective length =  $L/2$

And when made one end free then effective length =  $2L$

$$\text{Crippling load} = \frac{\pi^2 EI}{L_e^2}$$

$$\text{For case 1 } F = \frac{\pi^2 EI}{(0.5L)^2} = \frac{4\pi^2 EI}{L^2}$$

$$\text{For Case 2 Crippling load } F_2 = \frac{\pi^2 EI}{(2L)^2} = \frac{\pi^2 EI}{4L^2} = \frac{F}{16}$$

16. The compression members always tend to buckle in the direction of

- A. Axis load
- B. Perpendicular to the axis of load
- C. Minimum cross-section
- D. Least radius of gyration

Ans. D

Sol. M.I should be as maximum as possible to resist buckling.

So, chances of buckling is possible about axis having low Moment of Inertia.

17. The bar of a boring machine is 45 mm in diameter. During operation, the bar may be twisted through 0.01 radians and subjected to a shear stress of 45 MPa. What is the required length of the bar?

(take  $G = 0.84 \times 10^5 \text{ N/mm}^2$ )

- A. 380 mm
- B. 550 mm
- C. 420 mm
- D. 395 mm

Ans. C

Sol. From the equation to torsion:

$$\frac{T}{J} = \frac{\tau_{\max}}{R} = \frac{G\theta}{L}$$

$$\frac{45}{(45/2)} = \frac{0.84 \times 10^5 \times 0.01}{L}$$

$$2 = \frac{0.84 \times 10^5 \times 0.01}{L}$$

$$L = \frac{0.84 \times 10^5 \times 0.01}{2}$$

$$L = 420 \text{ mm}$$

18. Find the modulus of elasticity of a rod, which tapers uniformly from 30mm to 15mm diameter in a length of 300mm. The rod is subjected to axial load of 5kN and extension of rod is 0.022mm.

A.  $1.96789 \times 10^5 \text{ N/mm}^2$

B.  $2.145 \times 10^5 \text{ N/mm}^2$

C.  $1.92915 \times 10^5 \text{ N/mm}^2$

D.  $1.8976 \times 10^5 \text{ N/mm}^2$

Ans. C

Sol. Given, Large diameter,  $D_1 = 30\text{mm}$

Small diameter,  $D_2 = 15\text{mm}$

Length(L) = 300mm

Axial load(P) = 5kN = 5000N

Extension(dl) = 0.022mm

We know that extension for a tapered bar(dl) =

$$= \frac{4PL}{\pi E D_1 D_2}$$

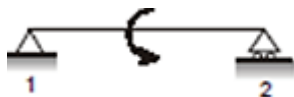
$$0.022 = \frac{4 \times 5000 \times 300}{\pi E (30)(15)}$$

$$E = 192915.08 \text{ N/mm}^2 = 1.92915 \times 10^5 \text{ N/mm}^2$$

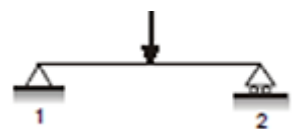
19. Match List-I with List-II and choose the correct answer using the codes given below:

List-I (Loading diagram)

A-

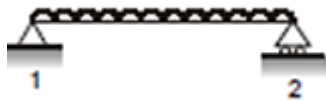


B-

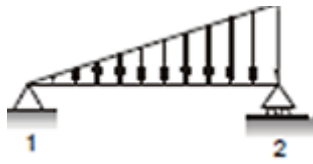


C-

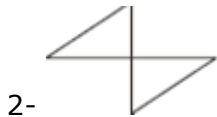




D-



List-II (Bending moment diagram)



A. A-4, B-2, C-1, D-3

B. A-5, B-1, C-4, D-3

C. A-2, B-5, C-3, D-1

D. A-2, B-4, C-1, D-3

Ans. D

Sol.

Load	Slope for shear force	Slope for bending Moment
<p>P</p>	<p>Constant</p>	<p>Linear</p>
<p>Uniformly distributed load</p>	<p>Linear</p>	<p>Parabolic</p>
<p>Uniformly varying load</p>	<p>Parabolic</p>	<p>Cubic</p>

20. A long column is most likely to fail by \_\_\_\_\_.

A. Crushing

B. Tension

C. Shearing

D. Buckling

Ans. D

Sol.

- Long column generally fail by the buckling which is the phenomenon of lateral or horizontal displacement of long columns, which cause their failure.

21. What is the application of determining principle stresses
- A. to ensue the material of same composition
  - B. to ensure the safety of structural component
  - C. (A) and (B) both
  - D. none of these

Ans. B

Sol. to ensure safety of structural component, each and every plane must have stress less than maximum permissible stress i.e. Principle stresses.

22. Consider the following theories of failure:
- A) Maximum stress theory
  - B) Maximum strain theory
  - C) Maximum shear stress theory
  - D) Maximum energy or distortion theory

The most suitable for ductile material is

- A. A and B
- B. A and C
- C. A and D
- D. C and D

Ans. D

Sol. 1. Maximum Principal Stress theory also known as RANKINE'S THEORY

2. **Maximum Shear Stress theory** or GUEST AND TRESCA'S THEORY

3. Maximum Principal Strain theory also known as St. VENANT'S THEORY

4. Total Strain Energy theory or HAIGH'S THEORY

5. **Maximum Distortion Energy theory** or VONMISES AND HENCKY'S THEORY "c" and "d" option is correct.

23. A spring has wire diameter  $d$  and coil diameter  $D$ . If  $d$  and  $D$  are halved, the resulting deflection will be \_\_\_\_\_.

- A. half of original deflection
- B. Twice of original deflection
- C. four times of original deflection
- D. one fourth of original deflection

Ans. B

Sol. Deflection is given by:

$$\delta = \frac{8PD^3n}{Gd^4}$$

Thus, Deflection is proportional to  $D^3/d^4$ .

When both  $d$  and  $D$  are halved:

$$\delta = \frac{8P\left(\frac{D}{2}\right)^3n}{G\left(\frac{d}{2}\right)^4} = 2\left(\frac{8PD^3n}{Gd^4}\right) = 2\delta$$



Sol.

$$\frac{T}{J} = \frac{\tau}{r} = \frac{G\theta}{l}$$

$$\frac{J}{r} = \frac{T}{\tau} = \frac{G\theta}{l}$$

$\frac{J}{r}$  = Torsional section modulus

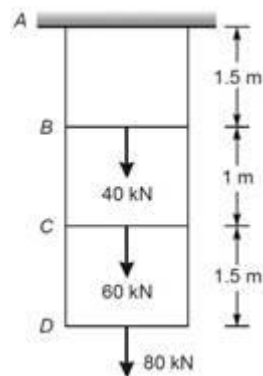
$$J = \frac{\pi(D_1^4 - D_2^4)}{32} = \frac{\pi(10^4 - 5^4)}{32} = 920.4$$

$$r = \frac{10}{2} = 5 \text{ cm}$$

So,

$$\frac{J}{r} = \frac{920.4}{5} = 184 \text{ cm}^3$$

28. A steel bar of 4 m length and uniform cross-sectional area of 1200 mm<sup>2</sup> is suspended vertically and loaded as shown in figure. The elongation of the bar will be [Take, E = 2.05 × 10<sup>5</sup> N/mm<sup>2</sup>]

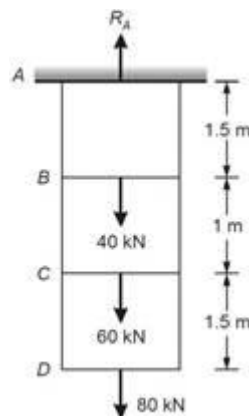


- A. 1.25 mm  
C. 3.15 mm

- B. 2.15 mm  
D. 4.25 mm

Ans. B

Sol.



$$R_A = 40 + 60 + 80 = 180 \text{ kN}$$

Force  $P_1$  on portion  $AB = 180$  kN (tensile)

Force  $P_2$  on portion  $BC = 180 - 40 = 140$  kN (tensile)

Force  $P_3$  on portion  $CD = 80$  kN (tensile)

$$\Delta = \frac{1}{AE}(P_1L_1 + P_2L_2 + P_3L_3)$$

$$\Delta = \frac{1}{1200 \times 2.05 \times 10^5} \times [180 \times 1500 + 140 \times 1000 + 80 \times 1500] \times 10^3$$

$$= \frac{530000 \times 10^3}{1200 \times 2.05 \times 10^5} = 2.15 \text{ mm}$$

29. The linear relation between the stress and strain of a material is valid until

- A. Fracture stress
- B. Elastic limit
- C. Ultimate stress
- D. Proportional limit

Ans. D

Sol. According to Hook's law stress is directly proportional to strain upto proportional limit.

30. If the principal stresses and the maximum shear stress are of equal magnitude in a Mohr's Circle, the state of stress can be termed as

- A. Isotropic
- B. Pure shear
- C. Uniaxial
- D. Generalized plane state of stress

Ans. B

Sol. When the Max shear stress =  $\sigma$ , principal stresses are  $+\sigma$  and  $-\sigma$ , the Mohr's circle is a circle of centre at origin and radius  $\sigma$  and that is pure shear state of stress.

31. Slenderness ratio of column is the ratio of \_\_\_\_\_.

- A. Length to its least radius of gyration
- B. Length to its maximum radius of gyration
- C. Square root of length to its least radius of gyration
- D. Square root of length to its maximum radius of gyration

Ans. A

Sol. Slenderness ratio is given by:

$$S = \frac{L_e}{K} = \frac{\text{Length of column}}{\text{Least radius of gyration}}$$

32. A hollow and solid shaft have same outer radii and the ratio of outer and inner radius of hollow shaft is 2:1. if both the shaft is made of same material ,then ratio of the torques of the hollow and solid shaft is

- A. 256:1
- B. 1:256
- C. 16:15
- D. 15:16

Ans. D

Sol. Given,

$T_{\max} = \text{same}$ ,

diameter ratio for hollow shaft  $D/d = 2$   
outer diameter of both shaft is same  
form the torsion equation

$$\frac{T}{J} = \frac{\tau_{max}}{R_0} = \frac{G\theta}{L}$$

$$T = \frac{J\tau_{max}}{R_0}$$

$$J_s = \frac{\pi}{32} D^4 \quad \& \quad J_H = \frac{\pi}{32} (D^4 - d^4)$$

$$\frac{T_s}{T_H} = \frac{J_s}{J_H} = \frac{\frac{\pi}{32} D^4}{\frac{\pi}{32} (D^4 - d^4)} = \frac{D^4}{(D^4 - d^4)}$$

$$\frac{T_s}{T_H} = \frac{D^4}{D^4 \left(1 - \frac{d^4}{D^4}\right)} = \frac{1}{\left(1 - \frac{d^4}{D^4}\right)} = \frac{1}{1 - \left(\frac{1}{2}\right)^4}$$

$$\frac{T_s}{T_H} = \frac{16}{15} \quad \text{or} \quad \frac{T_H}{T_s} = \frac{15}{16}$$

33. The stress in a body due to suddenly applied load compared to when it is applied gradually is \_\_\_\_\_.
- |              |               |
|--------------|---------------|
| A. same      | B. half       |
| C. two times | D. four times |

Ans. C

Sol. **Gradually applied load** is given as  $\sigma = (F/A)$  ----- (F is the gradually applied load)  
here, work done is given as  $(F \delta L) / 2$  and strain energy stored =  $(\sigma^2 / 2E) AL$   
Work done is equal to the strain energy stored.

$$(F \delta L) / 2 = (\sigma^2 / 2E) AL$$

$$\text{Therefore, } \sigma = (F/A) \text{ ----- (1)}$$

**Suddenly applied load** is given as  $\sigma = (2F/A)$ , here work done =  $(F \delta L)$

$$(F \delta L) = (\sigma^2 / 2E) AL$$

$$\text{Therefore, } \sigma = (2F/A) \text{ ----- (2)}$$

From (1) and (2), it can be concluded that **suddenly applied load is twice the gradually applied load.**

34. A column with highest equivalent length has \_\_\_\_\_.
- |   |
|---|
| A. Both ends fixed                        |
| B. Both ends hinged or pin-joined         |
| C. One end fixed, the other entirely free |
| D. One end fixed , other end hinged       |

Ans. C

Sol. A column with highest equivalent length has One end fixed, the other entirely free =  $2L$

Both fixed =  $L/2$

Both hinged =  $L$

One fixed on hinged =  $L/\sqrt{2}$

35. True stress represents the ratio of \_\_\_\_\_.

- A. Average load and average area
- B. Average load and maximum area
- C. Maximum load and maximum area
- D. Instantaneous load and instantaneous area

Ans. D

Sol. True stress is defined as the ratio of instantaneous force and instantaneous area.

36. If the principal stress in plane stress problem  $\sigma_1 = 200$  MPa,  $\sigma_2 = 50$  MPa, the magnitude of the maximum IN PLANE shear stress (in MPa) will be

- A. 125 MPa
- B. 100 MPa
- C. 75 MPa
- D. None of these

Ans. C

Sol. Given,

$$\sigma_1 = 200 \text{ MPa}, \sigma_2 = 50 \text{ MPa}$$

$$\text{In plane shear stress} = \frac{\sigma_1 - \sigma_2}{2} = \frac{200 - 50}{2} = 75 \text{ MPa}$$

37. If at a point in a body  $\sigma_x = 70$  MPa,  $\sigma_y = 60$  MPa and  $\tau_{xy} = -5$  MPa, then the radius of Mohr's circle is equal to.

- A.  $5\sqrt{5}$  MPa
- B.  $2\sqrt{5}$  MPa
- C.  $5\sqrt{2}$  MPa
- D. 25 MPa

Ans. C

Sol. Given,

$$\sigma_x = 70 \text{ Mpa}, \sigma_y = 60 \text{ Mpa}, \tau_{xy} = -5 \text{ Mpa}$$

Radius of Mohr's circle,

$$\begin{aligned} R &= \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \\ &= \sqrt{\left(\frac{70 - 60}{2}\right)^2 + (-5)^2} \\ &= \sqrt{25 + 25} \\ &= 5\sqrt{2} \text{ Mpa} \end{aligned}$$





Ans. D

Sol. A member subjected to only axial compressive force is called a strut. A strut may be horizontal, inclined or even vertical.

A column also primarily carries axial forces but may be subjected to bending and shear stresses as well.

42. A simply supported laterally loaded beam was found to deflect more than a specified value. Which of the following measures will reduce the deflection?
- A. Increase the area moment of inertia
  - B. Increase the span of the beam
  - C. Select a different material having lesser modulus of elasticity
  - D. Magnitude of the load to be increased

Ans. A

Sol.

We know, differential equation of flexure for the beam is,

$$EI \frac{d^2y}{dx^2} = M \Rightarrow \frac{d^2y}{dx^2} = \frac{M}{EI}$$

Integrating both sides,

$$\frac{dy}{dx} = \frac{1}{EI} \int M dx = \frac{1}{EI} Mx + c_1$$

Again integrating,

$$y = \frac{1}{EI} \left( \frac{Mx^2}{2} \right) + c_1x + c_2 \dots (i)$$

Where,  $y$  gives the deflection at the given point.

It is easily shown from the equation (i), If we increase the value of  $E$  &  $I$ , then deflection reduces

43. A prismatic bar of length 4m is subjected to an uniaxial pull of 100kN then the magnitude of product of change in diameter to its diameter will be (in  $\mu\text{m}$ ) take  $E = 200 \text{ GPa}$ ,  $\mu = 0.3$
- A. 0.763
  - B. 0.567
  - C. 0.190
  - D. Can not be determine

Ans. A

Sol. Given,  $L = 4\text{m}$ ,  $P = 100 \text{ kN}$ ,  $E = 200 \text{ GPa}$

$\mu = 0.3$

as we know that,

$$\Delta L = \frac{PL}{AE} = \frac{PL}{\frac{\pi}{4} d^2 E} \Rightarrow \Delta L = \frac{4PL}{\pi d^2 E}$$

$$\frac{\Delta d}{d} = -\mu \frac{\Delta L}{L}$$

$$\frac{\Delta d}{d} = -\mu \frac{4PL}{\pi d^2 E}$$

$$\Rightarrow (d \times \Delta d) = -\frac{\mu \times 4PL}{\pi E} = -\frac{0.3 \times 4 \times 100 \times 10^3 \times 4}{\pi \times 200 \times 10^9}$$

$$(d \times \Delta d) = -0.7639 \times 10^{-6} \text{m}$$

$$(d \times \Delta d) = -0.7639 \mu\text{m}$$

$$|d \times \Delta d| = 0.763 \mu\text{m}$$

44. If Poisson's ratio for a material is 0.5, then the elastic modulus for the material is  
 A. three times its shear modulus                      B. for times its shear modulus  
 C. equal to its shear modulus                              D. indeterminate

Ans. A

Sol.  $E = 2G(1 + \mu)$   
 $= 2G(1 + 0.5) = 3G$

45. A beam loaded by a 10kN UDL. The cross-section of the beam is 100×30×1000 mm(b×t×l). Determine the section modulus of the beam?  
 A. 9010 mm<sup>3</sup>    B. 10452 mm<sup>3</sup>  
 C. 12.45 mm<sup>3</sup>    D. 15000 mm<sup>3</sup>

Ans. D

Sol. Given: width = 100mm thickness = 30 mm

$$\text{Section modulus, } Z = \frac{\text{Moment of inertia}}{\text{Distance of outermost layer from Neutral axis}} = \frac{I}{Y_{\max}}$$

$$\text{Therefore, } I = \frac{bt^3}{12} = \frac{100 \times 30^3}{12} = 22.5 \times 10^4 \text{ mm}^4$$

$$Y_{\max} = 15\text{mm}$$

$$\therefore \text{Section modulus, } Z = \frac{22.5 \times (10)^4}{15} = 15000 \text{ mm}^3$$

46. The minimum axial compressive load, P required to initiate buckling for a pinned-pinned slender column with bending stiffness EI and length L is \_\_\_\_\_.  
 A.  $P = \frac{\pi^2 EI}{4L^2}$     B.  $P = \frac{\pi^2 EI}{L^2}$   
 C.  $P = \frac{3\pi^2 EI}{4L^2}$     D.  $P = \frac{4\pi^2 EI}{L^2}$

Ans. B

Sol. The Euler's minimum load required to buckle is given by:

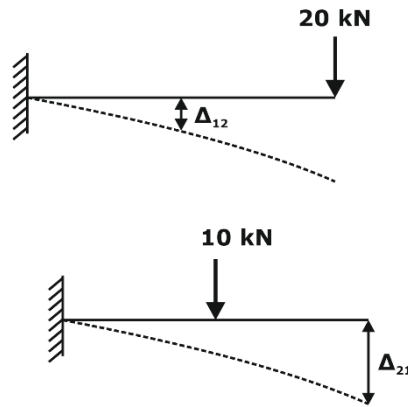
$$P_{cr} = \frac{\pi^2 EI}{L_e^2}$$

Where:  $L_e$  = effective length of the column.

Pinned-pinned column means hinged on both sides. Thus:  $L_e = l$

$$P_{cr} = \frac{\pi^2 EI}{L^2}$$





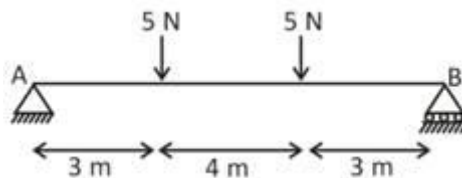
By Maxwell Reciprocal Theorem:

$$F_1 \times \Delta_{12} = F_2 \times \Delta_{21}$$

$$20 \times \Delta_{12} = 10 \times 2$$

$$\Delta_{12} = 1 \text{ mm}$$

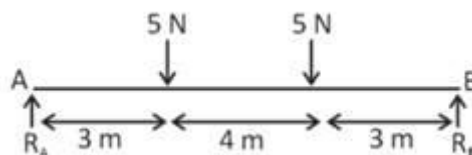
50. A simply supported beam AB is subjected to two point loads of 5N each as shown in the figure below. The bending moment at the mid-point of the beam is \_\_\_\_\_ kNm (correct to one decimal place)



- A. 5  
B. 15  
C. 10  
D. 0

Ans. B

Sol.



Calculating the support reactions,

Vertical force equilibrium

$$R_A + R_B = 10N$$

Moment about point A

$$R_B \times 10 = 5 \times 3 + 5 \times 7 = 15 + 35 = 50 \text{ kN}$$

$$R_B = 5N = R_A$$

Bending moment at the mid-point

$$BM = R_B \times 5 - 5 \times 2 = 5 \times 5 - 5 \times 2 = 15$$

$$BM = 25 - 10 = 15 \text{ N-m}$$

51. In a metal forming operation when the material has just started yielding, the principal stresses are  $\sigma_1 = +180 \text{ MPa}$ ,  $\sigma_2 = -100 \text{ MPa}$ ,  $\sigma_3 = 0$ . Following Von Mises criterion, the yield stress is \_\_\_\_\_ MPa.

- A. 245.76  
B. 240.12  
C. 248.57  
D. 251.98

Ans. A

Sol. **As per Von-Mises criteria**

$$(\sigma_1 - \sigma_2)^2 + (\sigma_1 - \sigma_3)^2 + (\sigma_2 - \sigma_3)^2 = 2\sigma_m^2$$

$$(180 - (-100))^2 + (180 - 0)^2 + (-100 - 0)^2 = 2\sigma_m^2$$

$$\sigma_m = 245.76 \text{ MPa}$$

52. For a power transmission shaft which transmits power P kW at N rpm, then the diameter of the shaft is proportional to.

- A.  $\left(\frac{P}{N}\right)^{1/3}$   
B.  $\left(\frac{P}{N}\right)^{1/2}$   
C.  $\left(\frac{P}{N}\right)^{2/3}$   
D.  $\frac{P}{N}$

Ans. A

Sol. Power =  $\frac{2\pi NT}{60}$

$$\therefore \frac{T}{J} = \frac{T}{r}$$

$$T = \frac{\pi}{16} d^3 \tau$$

$$P = \frac{2\pi N}{60} \times \frac{\pi}{16} d^3 \tau$$

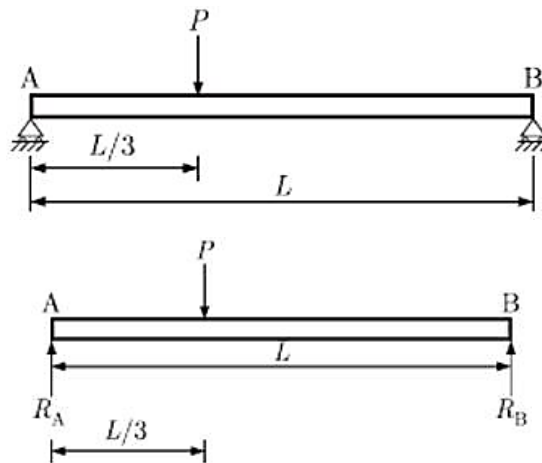
d is proportional to  $\left(\frac{P}{N}\right)^{1/3}$

53. A concentrated load of P acts on a simply supported beam of span L at a distance L/3 from the left support. The bending moment at the point of application of the load is given by

- A.  $\frac{PL}{3}$   
B.  $\frac{2PL}{3}$   
C.  $\frac{PL}{9}$   
D.  $\frac{2PL}{9}$

Ans. D

Sol. We know that, the simplest form of the simply supported on rollers at ends. The simply supported beam and the FBD shown in the Figure.



Where, are the reactions acting at the ends of the beam. In equilibrium condition of forces,

$$P = R_A + R_B \dots(i)$$

Taking the moment about point A,

$$R_B \times L = P \times \frac{L}{3}$$

$$R_B = \frac{P}{3}$$

From equation (i),

$$R_A = P - R_B = P - \frac{P}{3} = \frac{2P}{3}$$

Now bending moment at the point of application of the load

$$M = R_A \times \frac{L}{3} = \frac{2P}{3} \times \frac{L}{3} = \frac{2PL}{9}$$

$$\text{or, } M = R_B \times \frac{2L}{3} = \frac{2PL}{9}$$

54. For a circular shaft of diameter  $d$  subjected to torque  $T$ , the maximum value of the shear stress is.

A.  $\frac{64T}{\pi d^3}$

B.  $\frac{32T}{\pi d^3}$

C.  $\frac{16T}{\pi d^3}$

D.  $\frac{8T}{\pi d^3}$

Ans. C

Sol. From the equation of torsion

$$\frac{T}{J} = \frac{\tau_{\max}}{d/2}$$

$$\frac{T}{\pi d^4 / 32} = \frac{\tau_{\max}}{d/2}$$

$$\tau_{\max} = \frac{16T}{\pi d^3}$$







$$\frac{E}{2G} = \mu + 1 \quad \mu = \text{Poisson Ratio}$$

$$\mu = \frac{E}{2G} - 1 = \frac{200}{2 \times 66.67} - 1$$

$$= 1.49 - 1$$

$$= .49 \text{ approx}$$

$$= 0.50$$

61. All the failure theories give nearly the same result \_\_\_\_\_.
- A. When one of the principal stresses at a point is larger in comparison to the other
  - B. When shear stresses act
  - C. When both the principal stresses are numerically equal
  - D. For all situations of stress

Ans. A

Sol. When one of the principle stress at a point is large in comparison to the other, the situation resembles uniaxial tension test. Therefore all theories give nearly same result.

62. A cantilever beam of length L and flexural modulus EI is subjected to a point load P at the free end. The elastic strain energy stored in the beam due to bending (neglecting transverse shear)

- A.  $\frac{P^2L^3}{6EI}$
- B.  $\frac{P^2L^3}{3EI}$
- C.  $\frac{PL^3}{3EI}$
- D.  $\frac{PL^3}{6EI}$

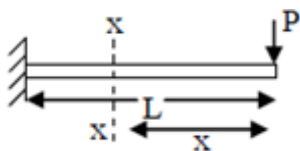
Ans. A

Sol.

$$M_x = -P \cdot x$$

$$\therefore U = \int_0^L \frac{M_x^2 dx}{2EI} = \frac{P^2 x^2 dx}{2EI}$$

$$U = \frac{P^2 L^3}{6EI}$$



63. A helical compression spring made of wire of circular cross-section is subjected to a compressive load. The maximum shear stress induced in the cross-section of the wire is 24 MPA. For the same compressive load, if both the wire diameter and the mean coil diameter are doubled, the maximum shear stress (in MPA) induced in the cross-section of the wire is \_\_\_\_\_

- A. 3
- B. 6
- C. 9
- D. 12

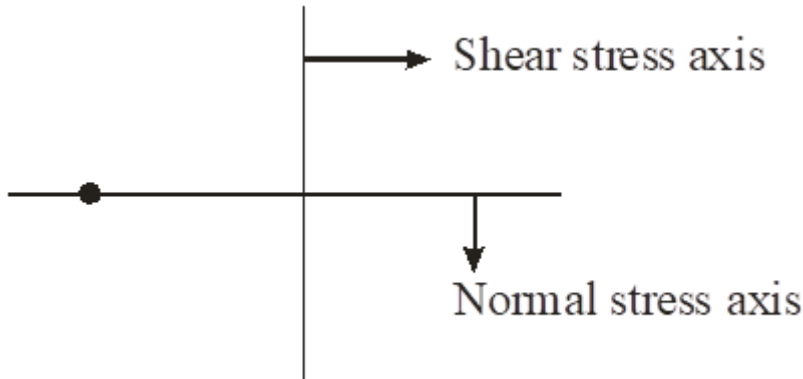
Ans. B



- A. A circle with centre at origin
- B. A circle with centre on x-axis
- C. A point circle on the normal stress axis
- D. A point circle on the shear stress axis

Ans. C

Sol.



A fluid element under static condition will have zero shear stress and equal compressive stresses will be present in all the directions, making the required Mohr's circle a point on the normal stress axis .

68. A thin cylinder of diameter 15 mm, thickness 3 mm, pressure 10 N/m<sup>2</sup> and Poisson's ratio 0.5, the longitudinal strain is \_\_\_\_\_.
- A. 37.5
  - B. 12.5
  - C. 0.0
  - D. Data insufficient

Ans. C

Sol. For thin cylinder longitudinal strain is given by:

$$\epsilon_l = \frac{\sigma_l}{E} - \mu \frac{\sigma_h}{E} = \frac{1}{E} \left( \frac{pD}{4t} - \mu \frac{pD}{2t} \right)$$

$$\epsilon_l = \frac{pD}{4tE} (1 - 2\mu)$$

Since, Poisson's ratio is 0.5.

$$\epsilon_l = \frac{pD}{4tE} (1 - 2 \times 0.5) = 0$$

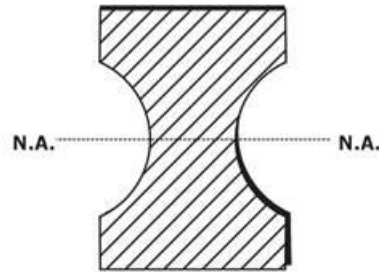
69. Consider the following theories of failure:
- A) Maximum stress theory
  - B) Maximum strain theory
  - C) Maximum shear stress theory
  - D) Maximum energy or distortion theory

The most suitable for ductile material is

- A. A and B
- B. A and C
- C. A and D
- D. C and D

Ans. D

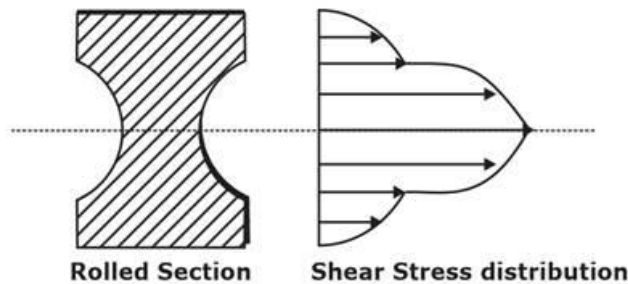
- Sol. 1. Maximum Principal Stress theory also known as RANKINE'S THEORY  
 2. **Maximum Shear Stress theory** or GUEST AND TRESCA'S THEORY  
 3. Maximum Principal Strain theory also known as St. VENANT'S THEORY  
 4. Total Strain Energy theory or HAIGH'S THEORY  
 5. **Maximum Distortion Energy theory** or VONMISES AND HENCKY'S THEORY "c" and "d" option is correct.
70. Which of the following is the correct shear stress distribution for the rolled section as shown in figure:



- A.
- B.
- C.
- D.

Ans. B

Sol. The shear stress distribution for a rolled section has been shown below:



71. A thin cylindrical pressure vessel with closed-ends is subjected to internal pressure. The ratio of circumferential (hoop) stress to the longitudinal stress is
- A. 0.25                                      B. 0.50  
 C. 1.0                                        D. 2.0

Ans. D

Sol. Circumferential stress:

$$\sigma_c = \frac{pD}{2t}$$

Longitudinal stress:

$$\sigma_l = \frac{pD}{4t}$$

where, p is internal pressure d is internal diameter t is thickness.

$$\frac{\sigma_c}{\sigma_l} = \frac{\frac{pD}{2t}}{\frac{pD}{4t}} = 2$$

72. The state of stress at a point under plane stress condition is  $\sigma_{xx} = 50$  MPa,  $\sigma_{yy} = 80$  MPa and  $\tau_{xy} = 30$  MPa. The diameter of Mohr's circle representing the given state of stress (in MPa) is \_\_\_\_\_.

- A. 33.5 MPa
- B. 53 MPa
- C. 67 MPa
- D. 78 MPa

Ans. C

Sol. Radius of Mohr's circle is given by:

$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$R = \sqrt{\left(\frac{50 - 80}{2}\right)^2 + (30)^2} = 33.5410 \text{ MPa}$$

Diameter of Mohr's circle :

$$D = 2R = 2 \times 33.5410 = 67.08 \text{ MPa}$$

73. For a bar subjected to moment  $M = 10x^2 + 21x + 20$ , find the shear force acting on the body at  $x=0$

- A. 10
- B. 20
- C. 21
- D. 51

Ans. C

Sol.  $F = dM / dx$

$$F = 20x + 21$$

At  $x=0$

$$F = 21$$

74. A beam is loaded as cantilever. If the load at the end is increased, the failure will occur \_\_\_\_.

- A. in the middle
- B. at the tip below the load
- C. at the support
- D. anywhere

Ans. C

Sol. we know that as per the bending equation,ie

$$\frac{M}{I} = \frac{\sigma}{y} = \frac{E}{R}$$

So as M ie bending moment increases, the stress also increases and the chances of failure increases with it.

Because maximum bending moment occur at fixed end. Hence (C) is correct.

75. At the neutral axis in a beam, there is

- A. Maximum tensile stress
- B. Maximum compressive stress
- C. No bending stress
- D. Always stress developed depending on load applied

Ans. C

Sol. At the neutral axis there is no bending stress.

We know bending equation

$$\frac{M}{I} = \frac{\sigma}{y} = \frac{E}{R}$$

Bending stress,  $\sigma = y \frac{E}{R}$

At neutral axis  $y = 0$ ,

$$\sigma = 0$$

76. The ratio of hoop stress to longitudinal stress in thin walled cylinders is:

- A. 1
- B. 1/2
- C. 2
- D. 1/4

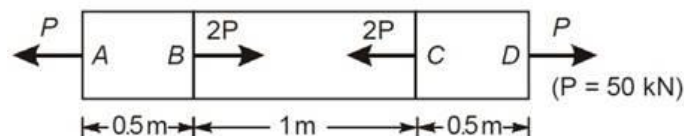
Ans. C

Sol. Hoop stress  $(\sigma_n) = \frac{pd}{2t}$

Longitudinal stress  $\sigma_l = \frac{pd}{4t}$

$$\frac{\sigma_n}{\sigma_l} = 2$$

77. A slender bar of 100 mm<sup>2</sup> cross-section is subjected to loading as shown in the figure. If the modulus of elasticity is taken as 200 × 10<sup>9</sup> Pa, then the elongation produced in the bar will be \_\_\_\_ mm.



- A. 0
- B. 0.5
- C. 0.75
- D. 1

Ans. A

Sol. Given,

Cross-section= 100 mm<sup>2</sup>,

modulus of elasticity =  $200 \times 10^9$  Pa

Elongation of the bar

$$= \sum \frac{PL}{AE}$$

$$= \frac{P \times 0.5}{AE} - \frac{P \times 1}{AE} + \frac{P \times 0.5}{AE}$$

$$= 0$$

78. In thin cylinder the hoop stress is 200 MPa then the maximum shear stress ( in plane) is equal to

- A. 100 MPa
- B. 50 MPa
- C. 200 MPa
- D. 400 MPa

Ans. B

Sol.

$$\sigma_H = 200 MPa$$

$$\sigma_L = \frac{\sigma_H}{2} = \frac{200}{2} = 100 MPa$$

$$\tau(\text{in plane}) = \frac{\sigma_H - \sigma_L}{2} = \frac{200 - 100}{2} = 50 MPa$$

79. In the calculation of induced shear stress in helical springs, the Wahl's correction factor is used to take care of

- A. combined effect of transverse shear stress and bending stress in the wire.
- B. combined effect of bending stress and curvature of the wire.
- C. combined effect of transverse shear stress and curvature of the wire.
- D. combined effect of torsional shear stress and transverse shear stress in the wire.

Ans. C

Sol.

- Wahl factor includes the effects of both direct shear and wire curvature. It is given by Wahl factor,

$$K = \frac{4C-1}{4C-4} + \frac{0.615}{C}$$

where C=Spring index= D/d

where D= coil diameter, d= wire diameter

80. If a part is constrained to move and heated, it will develop

- A. principal stress
- B. tensile stress
- C. compressive stress
- D. shear stress

Ans. C

Sol. Whenever a body is heated it expands and when allowed to cool it normally contracts. Its the natural behaviour of material. Hence compressive stress is the right answer.





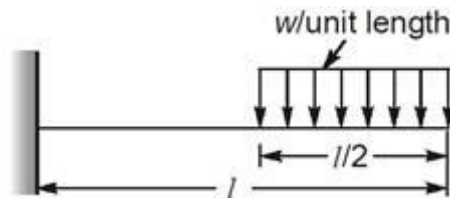


$$\frac{M}{I} = \frac{\sigma_b}{y}$$

$$\frac{20 \times 10^3}{\frac{(0.1)^4}{12}} = \frac{\sigma_b}{50 \times 10^{-3}}$$

$$(\sigma_b)_{\max} = 120 \text{ MPa}$$

87. A uniform cantilever beam with flexural rigidity EI is shown in figure. The bending deflection at the free end is



A.  $\frac{47Wl^4}{384EI}$

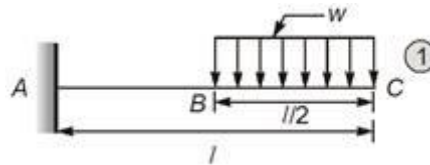
B.  $\frac{41Wl^4}{384EI}$

C.  $\frac{43Wl^4}{384EI}$

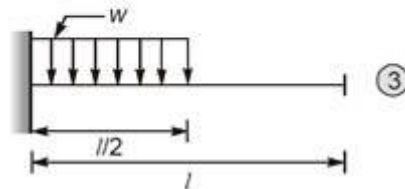
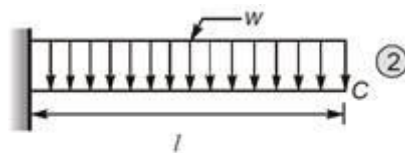
D.  $\frac{49Wl^4}{384EI}$

Ans. B

Sol.



By use of superposition principle



$$\delta_1 = \delta_2 - \delta_3$$

As we know that:

deflection at free end under UDL,  $\delta_2 = \frac{wL^4}{8EI}$

For case (3):

Deflection due to (3),  $\delta_3 = \frac{wa^4}{8EI} + \frac{wa^3}{6EI}(L - a)$

here,  $a = L/2$

$$\delta_3 = \frac{w\left(\frac{L}{2}\right)^4}{8EI} + \frac{w\left(\frac{L}{2}\right)^3}{6EI} \left(L - \frac{L}{2}\right) = \frac{7wL^4}{384EI}$$

$$\delta_1 = \frac{wL^4}{8EI} - \frac{7wL^4}{384EI} = \frac{41wL^4}{384EI}$$

88. Shear force in the beams can be defined as

- A. Rate of change of loading
- B. Rate of change of bending moment
- C. Rate of change concavity
- D. None

Ans. B

Sol. Shear force is equal to the rate of change of bending moment. The slope of the bending moment diagram at any point gives the shear force at that point.

89. Ratio of maximum shear stress developed in a rectangular cross-section beam to that developed in a circular cross-section beam for the same average shear stress is

- A. 1.33
- B. 1.125
- C. 2.5
- D. 1.5

Ans. B

Sol.

$$\text{maximum shear stress in rectangular beam} = \frac{3}{2} \times \text{average shear stress}$$

$$\text{maximum shear stress in circular beam} = \frac{4}{3} \times \text{average shear stress}$$

$$\frac{\text{maximum shear stress in rectangular beam}}{\text{maximum shear stress in circular beam}} = \frac{\frac{3}{2} \times \text{average shear stress}}{\frac{4}{3} \times \text{average shear stress}}$$

$$\frac{\text{maximum shear stress in rectangular beam}}{\text{maximum shear stress in circular beam}} = \frac{9}{8} = 1.125$$

90. A thin cylinder of inner radius 500 mm and thickness 5 mm is subjected to an internal gauge pressure of 5 MPa. The average hoop stress in MPa is

- A. 100
- B. 250
- C. 500
- D. 1000

Ans. C

Sol. Given,

Inner radius = 500 mm

Thickness = 5 mm



93. The power transmitted by two shafts A and B is 10 kW and 30Hp respectively. Keeping all the other conditions same what is the ratio between the torques of A and B.

- A. 4/9  
 B. 1000/3  
 C. 45/2  
 D. 2/45

Ans. A

Sol.

$$P_A = \frac{2\pi NT_A}{60} = 10 \times 10^3$$

$$P_B = \frac{2\pi NT_B}{60} = 30 \times 750$$

Thus,

$$T_A/T_B = 4/9$$

94. Modulus of resilience in a member is stored strain energy \_\_\_\_\_.

- A. per unit volume  
 B. in whole volume  
 C. per unit area  
 D. per unit length

Ans. A

Sol.

- The modulus of resilience is defined as the maximum energy that can be absorbed per unit volume without creating a permanent distortion.
- The modulus of resilience is the area under the curve up to the yield strength.

95. A 5 m long and 60 mm diameter steel bar is subjected to a tensile load of 100 kN. If the modulus of elasticity for the bar material is 210 GPa, then the modulus of resilience is

- A. 0.037  
 B. 0.3667  
 C. 0.0029  
 D. 0.0297

Ans. C

Sol. Cross section area of bar =  $A = \frac{\pi}{4}(60)^2 = 2827.43 \text{ mm}^2$

Strain energy is given by,

$$U = \frac{P^2 L}{2AE} = \frac{(100 \times 10^3)^2 \times 5000}{2 \times 2827.43 \times 210 \times 10^3} = 42104.5 \text{ N-mm} = 42.1 \text{ J}$$

Now, modulus of resilience,

$$u = \frac{U}{V} = \frac{42104.5}{2827.43 \times 5000} = 0.002978$$

96. Consider a beam with circular cross-section of diameter  $d$ . The ratio of the second moment of area about the neutral axis to the section modulus of the area is.

- A.  $\frac{d}{2}$   
 B.  $\frac{\pi d}{2}$   
 C.  $d$   
 D.  $\pi d$

Ans. A

Sol.

