

# ESE (Mains) 2019 Electromagnetic

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## Important Questions with Solutions



**EMT**

1. Two homogeneous isotropic dielectrics are separated by plane  $z = 0$ .

For  $z \geq 0$  ;  $\epsilon_r = 4$  and  $E = 3\hat{x} + 4\hat{z}$  kV/m

If  $\epsilon_r = 3$  for  $z \leq 0$  then find,

- A. E for  $z \leq 0$
- B. The angles that electric field makes with the normal to the plane  $z = 0$  for  $z \geq 0$  and for  $z \leq 0$
- C. The energy densities in both the dielectrics
- D. The energy within a cube of side of 4 m and centred at  $(1, -3, 5)$

Sol.

A) Let  $\epsilon_{r1} = 4$  and  $E_1 = 3\hat{x} + 4\hat{z}$

$\epsilon_{r2} = 3$

Since mediums are separated by  $z = 0$  plane  $\hat{n}_1$  will be normal to the plane

$$\therefore E_{n1} = 6$$

$$\& E_{t1} = E_1 - E_{n1}$$

$$\therefore E_{t1} = 3\hat{x} + 4\hat{z} - 6\hat{z} = 3\hat{x} - 2\hat{z}$$

Now  $E_{t2} = E_{t1}$

$$\therefore E_{t2} = 3\hat{x} - 2\hat{z} \quad \dots(i)$$

and  $D_{n2} = D_{n1}$

$$\therefore \epsilon_{r2} E_{n2} = \epsilon_{r1} E_{n1}$$

$$\therefore E_{n2} = \frac{4}{3} \cdot 6 = 8$$

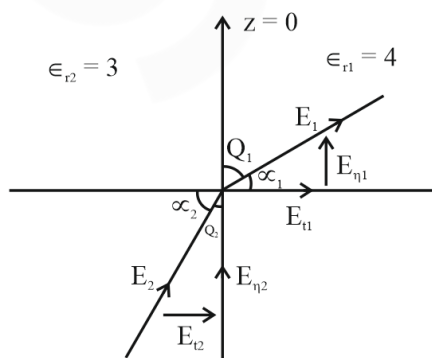
$$\therefore E_{n2} = 8 \quad \dots(ii)$$

Adding (i) and (ii)

$$E_2 = E_{t1} + E_{n2}$$

$$\therefore E_2 = 3\hat{x} - 2\hat{z} + 8\hat{z} = 3\hat{x} + 6\hat{z} \text{ kV/m For } z \leq 0$$

B)



Now

$$E_{n1} = 6$$

$$\therefore |E_{n1}| = 6$$

and  $E_{t1} = 3\hat{x} - 2\hat{z}$

$$\therefore |E_{t1}| = \sqrt{3^2 + 4^2}$$

$$\therefore |E_{t1}| = 5$$

$$\therefore \tan Q_1 = \frac{E_{t1}}{E_{n1}}$$

$$= \frac{5}{6}$$

$$\therefore Q_1 = 39.80^\circ$$

$$\therefore \alpha_1 = 90 - Q_1$$

$$= 90 - 39.80$$

$$\therefore \alpha_1 = 50.19^\circ$$

So  $E_1$  makes  $50.19^\circ$  angle with the normal to  $z = 0$  plane

$$E_{n2} = 8$$

$$\therefore |E_{n2}| = 8$$

and  $E_{t2} = 3\hat{x} - 2\hat{z}$

$$\therefore |E_{t2}| = \sqrt{3^2 + 4^2}$$

$$\therefore |E_{t2}| = 5$$

$$\therefore \tan Q_2 = \frac{E_{t2}}{E_{n2}} = \frac{5}{8}$$

$$\therefore Q_2 = 32^\circ$$

$$\therefore \alpha_2 = 90 - Q_2$$

$$= 90 - 32$$

$$\therefore \alpha_2 = 58^\circ$$

So  $E_2$  makes  $58^\circ$  angle with the normal to  $z = 0$  plane.

C) The energy density is given by,

$$WE_1 = \frac{1}{2} \epsilon_1 |E_1|^2$$

$$= \frac{1}{2} \times 4 \times \frac{1}{36\pi \times 10^9} \times (3^2 + 4^2 + 6^2) \times 10^6$$

$$\therefore WE_1 = 1.07 \text{ mJ/m}^3$$

$\therefore$  Energy density for  $z \geq 0$  will be  $1.07 \text{ mJ/m}^3$

$$\text{now } WE_2 = \frac{1}{2} \epsilon_2 |E_2|^2$$

$$= \frac{1}{2} \times 3 \times \frac{1}{36\pi \times 10^9} \times (3^2 + 4^2 + 8^2) \times 10^6$$

$$\therefore WE^2 = 1.4 \text{ mJ/m}^3$$

$\therefore$  Energy density for  $z \leq 0$  will be  $1.4 \text{ mJ/m}^3$

D) Given cube has centre  $(1, -3, 5)$  and it has side of  $4 \text{ m}$  so it completely lies for  $z \geq 0$

$\therefore$  the cube will have energy density  $1.07 \text{ mJ/m}^3$

As it has side of  $4 \text{ m}$

It will cover the region

$$-1 \leq x \leq 3 ; -5 \leq y \leq -1 ; 3 \leq z \leq 7$$

$$\therefore WE_2 = \text{○}$$

$$= \int_{x=-1}^3 \int_{y=-5}^{-1} \int_{z=3}^7 WE_2 \, dx \, dy \, dz$$

$$= 1.07 \times 4 \times 4 \times 4 \times 10^{-3}$$

$$\therefore WE = 69.03 \text{ mJ}$$

2. The magnetic field of a plane was travelling in free space is given by,

$$H_s = 0.05 \cos(\omega t - j6\pi z) (\hat{a}_y - j\hat{a}_x, \text{ A/m})$$

then find

A. Frequency and direction of propagation

B. Corresponding electric field vector

C. polarization of the wave

D. time average power density associated with wave

Sol.

$$A) H_s = 0.05 \cos(\omega t - j6\pi z) (\hat{a}_y - j\hat{a}_x, \text{ A/m})$$

A/m

$\therefore$  the wave is travelling along +ve z direction and  $\beta = 6\pi$

$$\text{now } V_p = \frac{\omega}{\beta}$$

As the wave is travelling through free space

$$V_p = \frac{\omega}{\beta} = 3 \times 10^8$$

$$\therefore \omega = 6\pi \times 3 \times 10^8$$

$$\therefore f = 9 \times 10^8$$

$\therefore$  Frequency =  $900 \text{ MHz}$

$$B) \text{ Now } H_s = 0.05 \cos(\omega t - j6\pi z) (\hat{a}_y - j\hat{a}_x)$$

$$\therefore H_s = 0.05 \cos(\omega t - j6\pi z) \hat{a}_y$$

$$- 0.05j \cos(\omega t - j6\pi z) \hat{a}_x$$

$$\text{let } H_1 = 0.05 \cos(\omega t - j6\pi z) \hat{a}_y$$

$$\text{and } H_2 = -0.05j \cos(\omega t - j6\pi z) \hat{a}_x$$

$$\text{now } \frac{|E|}{|H|} = 120\pi \text{ and } \bar{E} \times \bar{H} = \bar{P}$$

$$\therefore |E_1| = 0.05 \times 120\pi = 18.8$$

$\therefore E_1$  direction =  $H_1$  direction  $\times$  propagation direction

$$= \hat{a}_y \hat{a}_z$$

$$\therefore E_1 \text{ direction} = \hat{a}_z$$

$$\therefore E_1 = 18.8 \cos(\omega t - j6\pi z) \hat{a}_z$$

Similarly

$$|E_2| = 0.05 \times 120\pi = 18.8$$

And  $E_2$  direction =  $H_2$  direction  $\times$  propagation direction =  $-j(\hat{a}_y \hat{a}_z)$

$$\therefore E_2 \text{ direction} = \hat{a}_x$$

Now  $E = E_1 + E_2$

$$\therefore E = 18.8 \cos(\omega t - j6\pi z) (\hat{a}_z + \hat{a}_x)$$

$$C) E = 18.8 \cos(\omega t - j6\pi z) (\hat{a}_z + \hat{a}_x)$$

We calculate polarization at  $z = 0$

$$\therefore E(0, t) = 18.8 \cos(\omega t) (\hat{a}_z + \hat{a}_x)$$

$$\therefore E(0, t) = 18.8 \cos \omega t (\hat{a}_z + \hat{a}_x)$$

As  $E_1 = E_2$  it will be circular polarization let's draw E vector at different time intervals.

$$\text{At } t = 0 \quad E = 18.8 (\hat{a}_z + \hat{a}_x)$$

$$\text{At } t = T/8$$

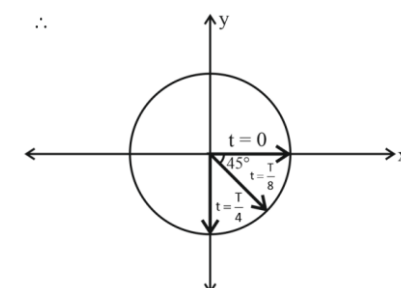
$$E = 18.8 \cos\left(\frac{2\pi}{T} \times \frac{T}{8}\right) \hat{a}_x - 18.8 \sin\left(\frac{2\pi}{T} \times \frac{T}{8}\right) \hat{a}_y$$

$$E = 18.8 \left( \frac{1}{\sqrt{2}} \hat{a}_x - \frac{1}{\sqrt{2}} \hat{a}_y \right)$$

$$\text{At } t = T/4$$

$$E = 18.8 \cos\left(\frac{2\pi}{T} \times \frac{T}{4}\right) \hat{a}_x - 18.8 \sin\left(\frac{2\pi}{T} \times \frac{T}{4}\right) \hat{a}_y$$

$$E = -18.8 \hat{a}_y$$



∴ It is left circular polarization.  
 D) Time average power density associated with wave is

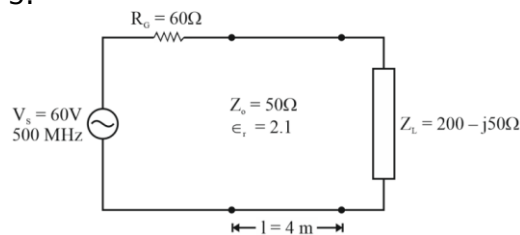
$$P = \frac{1}{2} (\mathbf{E}_s \times \mathbf{H}_s^*)$$

$$= \frac{1}{2} \times 18.8 \left( \hat{y} \times \hat{z} \right)$$

$$= \frac{0.94}{2} \left( \hat{y} \times \hat{z} \right)$$

$$P = 0.94 \hat{x}$$

3.



For the circuit as shown above calculate  
 A. Reflection co-efficient and VSWR  
 B. Input impedance seen by transmitter  
 C. The time averaged power delivered to the transmission line by the transmitter  
 D. The time averaged power delivered to antenna  
 E. Total power supplied by the transmitter

Sol.

A) Reflection co-efficient ( $\Gamma$ )

$$\Gamma = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{(200 - j50) - 50}{(200 - j50) + 50}$$

$$= 0.6154 - j0.0769$$

$$\therefore \Gamma = 0.6202 \angle -0.1244$$

$$\therefore |\Gamma| = 0.6202$$

$$VSWR = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

$$= \frac{1 + 0.6202}{1 - 0.6202}$$

$$\therefore VSWR = 4.27$$

B) Now  $V_p = \frac{\omega}{\beta}$

$$\therefore \beta = \frac{\omega}{V_p} = \frac{2\pi \times f}{V_p}$$

$$= \frac{2\pi \times 5 \times 10^8 \times \sqrt{2.1}}{3 \times 10^8}$$

$$\therefore \beta = 15.18 \text{ rad/m}$$

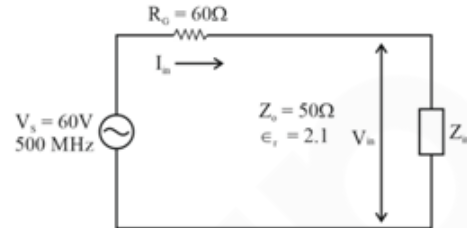
Now

$$Z_{in} = Z_0 \cdot \frac{Z_L \cos \beta l + j Z_0 \sin \beta l}{Z_0 \cos \beta l + j Z_L \sin \beta l}$$

$$= 50 \cdot \frac{(200 - j50) \cos(15.18 \times 4) + j50 \sin(15.18 \times 4)}{50 \cos(15.18 \times 4) + (200 - j50) \sin(15.18 \times 4)}$$

$$Z_{in} = 14.664 - j24.17 \Omega$$

C) Equivalent circuit can be drawn as,



$$\therefore V_{in} = V_s \cdot \frac{Z_{in}}{Z_{in} + R_G}$$

$$= 60 \times \frac{14.664 - j24.17}{14.664 - j24.17 + 60}$$

$$\therefore V_{in} = 16.3574 - j14.127V$$

$$\therefore |V_{in}| = 21.613 \angle -40.81^\circ$$

$$\therefore |V_{in}| = 21.613 \text{ V}$$

$$\text{now } I_{in} = \frac{V_{in}}{Z_{in}}$$

$$= \frac{21.613 \angle -40.81^\circ}{14.664 - j24.17}$$

$$I_{in} = 0.655 + j0.298$$

$$\therefore |I_{in}| = 0.7 \angle 20.8^\circ$$

$$\therefore |I_{in}| = 0.7 \text{ A}$$

Now power will be dissipated only across resistive part of the load

$$= \frac{1}{2} \times (I_{in})^2 \times \text{Real}(Z_{in})$$

$$\therefore P_{in} = \frac{1}{2} \times (0.7)^2 \times 14.664$$

$$\therefore P_{in} = 3.592 \text{ watt}$$

D) As the transmission line is lossless, total power delivered to the transmission line will be completely delivered to the antenna. The time average power delivered to the antenna is 3.592 watt.

E) Power dissipated in internal impedance  $R_G$  is

$$P_G = \frac{1}{2} \times (I_{in})^2 \times R_G$$

$$= \frac{1}{2} \times (0.7)^2 \times 60$$

$$\therefore P_G = 14.7 \text{ watt}$$

F) Total power supplied by the transmitter will be,

$$P_T = P_{in} + P_G$$

$$= 3.592 + 14.7$$

$$P_T = 18.292 \text{ watt}$$

4. A. Define dominant mode in a rectangular waveguide and find the power carried by the dominant mode for  $a > b$  by using transverse components.  
 B. Plot the  $TE_{10}$  mode and how to extract the  $TE_{10}$  mode effectively.

Sol.

A) Dominant mode: The mode which is having highest cut off wave length (or) lowest cut off frequency.

$$\lambda_C = \frac{2ab}{\sqrt{(mb)^2 + (na)^2}}$$

Lowest TM mode is  $TE_{11}$

$$\therefore \lambda_{CTM_{11}} = \lambda_{CTE_{11}} = \frac{2ab}{\sqrt{b^2 + a^2}}$$

$$\lambda_{CTE_{01}} = 2b$$

$$\lambda_{CTE_{10}} = 2a$$

As  $a > b$  i.e.,  $TE_{10}$  is the dominant mode  
 Field components for  $TE_{10}$

$$H_Z = C \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right)$$

$$E_X = -\frac{j\omega\mu}{h^2} \frac{\partial H_Z}{\partial y}$$

$$= \frac{j\omega\mu}{h^2} \frac{n\pi}{b} C \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right)$$

$$E_Y = \frac{j\omega\mu}{h^2} \frac{\partial H_Z}{\partial x}$$

$$= \frac{-j\omega\mu}{h^2} \frac{m\pi}{a} C \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right)$$

$$H_X = -\frac{\bar{\gamma}}{h^2} \frac{\partial H_Z}{\partial x}$$

$$= \frac{\bar{\gamma}}{h^2} \left(\frac{m\pi}{a}\right) C \sin\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right)$$

$$H_Y = -\frac{\bar{\gamma}}{h^2} \frac{\partial H_Z}{\partial y}$$

$$= \frac{\bar{\gamma}}{h^2} \left(\frac{n\pi}{b}\right) C \cos\left(\frac{m\pi}{a}x\right) \sin\left(\frac{n\pi}{b}y\right)$$

For,  $TE_{10} \Rightarrow H_z = C \cos\left(\frac{\pi}{a}x\right)$

and  $E_x = H_y = 0$

$$E_y = \frac{-j\omega\mu}{h^2} C \left(\frac{\pi}{a}\right) \sin\left(\frac{\pi}{a}x\right)$$

$$H_x = \frac{j\bar{\beta}}{h^2} C \left(\frac{\pi}{a}\right) \sin\left(\frac{\pi}{a}x\right)$$

Power carried by waveguide

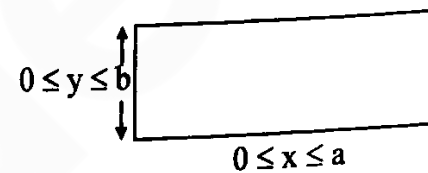
$$P = \int \vec{E} \times \vec{H} \cdot \hat{z} \, dx \, dy$$

$$\bar{P} = \frac{1}{2} \text{Re}[\bar{E} \times \bar{H}^*]$$

$$= \frac{1}{2} \text{Re} \left[ \frac{-j\omega\mu}{h^2} C \left(\frac{\pi}{a}\right) \sin\left(\frac{\pi}{a}x\right) \hat{y} \times \hat{x} \frac{j\bar{\beta}}{h^2} C \left(\frac{\pi}{a}\right) \sin\left(\frac{\pi}{a}x\right) \right]$$

$$\bar{P} = \frac{\bar{\beta}}{2} \frac{1}{\omega\mu} \frac{(\omega\mu)^2 C^2 \left(\frac{\pi}{a}\right)^2}{(h^2)^2} \sin^2\left(\frac{\pi}{a}x\right) \hat{z}$$

$$P = \frac{E_{\max}^2}{2Z_{TE}} \sin^2\left(\frac{\pi}{a}x\right) \hat{z}$$



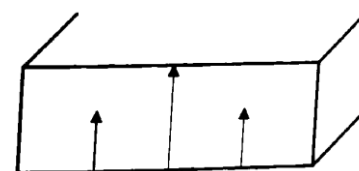
$$P = \int_0^a \int_0^b \sin^2\left(\frac{\pi}{a}x\right) dx \, dy$$

$$= \frac{E_{\max}^2}{2Z_{TE}} \times b \times \frac{a}{2}$$

$$\therefore P_{TE_{10}} = \frac{E_{\max}^2}{4Z_{TE}} ab$$

B) We have

$$E_y \propto \sin\left(\frac{\pi}{a}x\right)$$



As the maximum E is existing at midpoint of the broader dimension, it is effective if making use of probe or E-coupling.

5. A. Find the radiation efficiency of an Hertzian dipole metal wire having radius 1.8 mm, length 2 meter and  $\sigma = 6 \times 10^9$  s/m and it is operating at frequency of 2 MHz.

B. An end-fire array consists of  $\lambda/2$  radiations with axes at right angles to the line of the array required to have a power gain of 30. Determine the array length and the width of a major lobe between the nulls.

Sol.

A) For Hertzian dipole, Radiation resistance ( $R_r$ )

$$R_r = 80\pi^2 \left( \frac{dl}{\lambda} \right)^2$$

$$= 80\pi^2 \left( \frac{dl f}{c} \right)^2$$

$$= 80\pi^2 \left( \frac{2 \times 2 \times 10^6}{3 \times 10^8} \right)^2$$

$$R_r = 0.14 \Omega$$

And loss resistance ( $R_L$ )

$$R_L = \frac{dl}{2\pi a} \sqrt{\frac{\pi f \mu}{\sigma}}$$

$$\text{Now } dl = 2\text{m, } a = 1.8 \times 10^{-3},$$

$$\mu = 4\pi \times 10^{-7}$$

$$f = 2 \times 10^6, \sigma = 6 \times 10^9$$

$$\therefore R_L = \frac{2}{2\pi \times 1.8 \times 10^{-3}} \times \sqrt{\frac{\pi \times 2 \times 10^6 \times 4\pi \times 10^{-7}}{6 \times 10^9}}$$

$$\therefore R_L = 6.41 \times 10^{-3} \Omega$$

$$\therefore R_L = 0.00641 \Omega$$

$\therefore$  Radiation efficiency ( $\eta$ )

$$\eta = \frac{R_r}{R_r + R_L}$$

$$= \frac{0.14}{0.14 + 0.00641}$$

$$\therefore \eta = 0.9561$$

$\therefore$  Radiation efficiency = 95.61%

B) For an end fire array

$$D = 4 \left( \frac{L}{\lambda} \right)$$

$$30 = 4 \left( \frac{L}{\lambda} \right)$$

$$\therefore L = 7.5\lambda$$

$\therefore$  Array length =  $7.5\lambda$

Now width of a major lobe between the nulls is given as,

$$\text{BWFN} = 114.6 \sqrt{\frac{2}{L/\lambda}}$$

$$= 114.6 \sqrt{\frac{2}{7.5}}$$

$$\therefore \text{BWFN} = 59.18^\circ$$

$\therefore$  Width of major lobe between the nulls is  $59.18^\circ$ .

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