

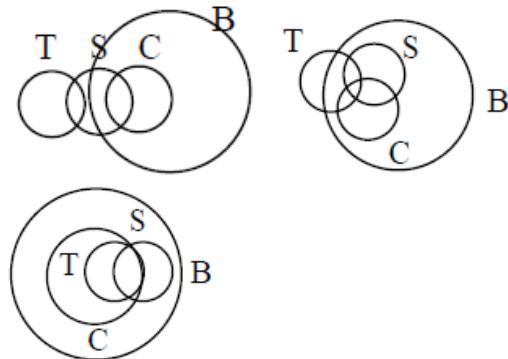
Solutions

General Aptitude

1. Ans. A.

Hurtful would be best option as person is complaining about her.

2. Ans. B.



3. Ans. B.

Given 40% of deaths on city roads are drunken driving

$$\text{w.k.t in pie chart } 100\% \rightarrow 360^\circ \quad 1\% \rightarrow \left(\frac{360}{100}\right) \quad 40\% \rightarrow$$

$$\left(\frac{360}{100}\right) \times 40 \quad 40\% \rightarrow 144^\circ$$

4. Ans. D.

Let H is house hold consumption and P is the other consumption.

Given

$$H \times 0.8 + P \times 1.7 = (H + P) \times 0.75$$

Ratio is negative.

5. Ans. A.

Past Tense is used.

6. Ans. D.

Option D is correct according to the passage

7. Ans. A.

No. of sub groups such that every sub group has at least one Indian

$$\begin{aligned}
 &= \underbrace{3C_1}_{\text{Only Indians}} + \underbrace{3C_2}_{\text{One Indian & remaining Chinese}} + \underbrace{3C_3}_{\text{One Indian & remaining Chinese}} \\
 &+ \underbrace{3C_2 \times 3C_1}_{\text{2 Indians & remaining Chinese}} + \underbrace{3C_3 \times 3C_1}_{\text{2 Indians & remaining Chinese}} + \underbrace{3C_2 \times 3C_2}_{\text{3 Indians & remaining Chinese}} + \underbrace{3C_3 \times 3C_2}_{\text{3 Indians & remaining Chinese}} + \underbrace{3C_3 \times 3C_3}_{\text{3 Indians & remaining Chinese}}
 \end{aligned}$$

$$= 7 + 9 + 9 + 3 + 6 + 9 + 9 + 3 + 3 + 1 = 56.$$

Alternate method

Sub groups containing only Indians

$$= 3C_1 + 3C_2 + 3C_3 = 3 + 3 + 1 = 7$$

Subgroups containing one Indian and rest Chinese

$$= 3C_1 [3C_1 + 3C_2 + 3C_3] = 3[3 + 3 + 1] = 21$$

Sub groups containing two Indian and remaining Chinese

$$3C_2 [3C_1 + 3C_2 + 3C_3] = 21$$

Sub groups containing three Indian and remaining Chinese

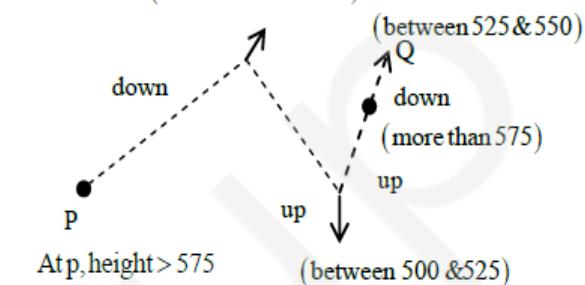
$$3C_3 [3C_1 + 3C_2 + 3C_3] = 7$$

$$\therefore \text{Total no. of sub group} = 7 + 21 + 21 + 7 = 56$$

8. Ans. C.

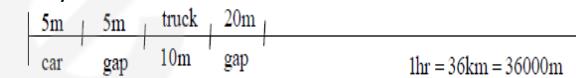
Down- up-Down

(between 475 & 500)



9. Ans. A.

Given speeds both car & Truck = 36 km/hour
They travel in 1 hr = 36 km = 36000 m.



\therefore Maximum no. of vehicles than can use the bridge in I

$$\text{hour} = \frac{36000 \text{m}}{50 \text{m}} = 720 \times 2 = 1440 \text{ vehicles}$$

Alternate method

Length of truck + gap required = 10 + 20 = 30m

Length of car + gap required = 5 + 15 = 20m

Alternative pairs of Truck and car needs 30 + 20 = 50 m.

Let 'n' be the number of repetition of (Truck + car) in 1

hour (3600 sec).

Given speed 36km /hr 10m /sec

$$\frac{50m \times n}{3600 \text{sec}} = 36 \text{km / hr}$$

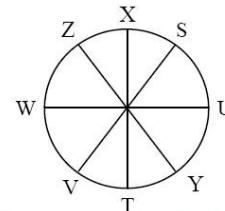
$$\Rightarrow \frac{50n}{3600} \text{m / sec} = 10 \text{m / sec}$$

$$\Rightarrow n = \frac{36000}{50} = 720 (\text{Truck + car})$$

So, 720 Truck car passes 720 2 1440 vehicles.

10. Ans. A.

Following circular seating arrangement can be drawn.



Only one such arrangement can be drawn.
The person on third to the left of V is X.

Electronics & Communications

1. Ans. C.

$$f_{clock} = 5 \text{ MHz}; T_{clock} = 0.2 \times 10^{-6} \text{ sec}$$

$$T_{execution} = 1.4 \mu\text{s}$$

$$\text{No. of T-state required} = \frac{1.4}{0.2} = 7$$

2. Ans. A.

For an input-output relation if the present output depends on present and past input values then the given system is "Causal".

For the given relation,

$$y[n] = \begin{cases} n|x[n]| & \text{for } 0 \leq n \leq 10 \\ x[n]-x[n-1] & \text{otherwise} \end{cases}$$

For n ranging from 0 to 10 present output depends on present input only.

At all other points present output depends on present and past input values.

Thus the system is "Causal".

Stability

If $x[n]$ is bounded for the given finite range of n i.e. $0 < n < 10$ $y[n]$ is also bounded.

Similarly $x[n]-x[n-1]$ is also bounded at all other values of n

Thus, the system is "stable".

3. Ans. B.

$$y_1 = 1, y_2 = x, y_3 = x^2$$

Consider

$$\begin{vmatrix} y_1 & y_2 & y_3 \\ y'_1 & y'_2 & y'_3 \\ y''_1 & y''_2 & y''_3 \end{vmatrix} = \begin{vmatrix} 1 & x & x^2 \\ 0 & 1 & 2x \\ 0 & 0 & 2 \end{vmatrix} = 2 \begin{vmatrix} 1 & x \\ 0 & 1 \end{vmatrix} = 2 \neq 0$$

$\Rightarrow y_1, y_2, y_3$ are linearly independent $\forall x$

4. Ans. C.

$$A = \begin{vmatrix} 1 & 2 & 3 & 4 & 5 \\ 5 & 1 & 2 & 3 & 4 \\ 4 & 5 & 1 & 2 & 3 \\ 3 & 4 & 5 & 1 & 2 \\ 2 & 3 & 4 & 5 & 1 \end{vmatrix}$$

For eigen values (λ), $|A - \lambda I| = 0$

$$\begin{vmatrix} 1-\lambda & 2 & 3 & 4 & 5 \\ 5 & 1-\lambda & 2 & 3 & 4 \\ 4 & 5 & 1-\lambda & 2 & 3 \\ 3 & 4 & 5 & 1-\lambda & 2 \\ 2 & 3 & 4 & 5 & 1-\lambda \end{vmatrix} = 0$$

$$R_1 \rightarrow R_1 + R_2 + R_3 + R_4 + R_5$$

$$\Rightarrow \begin{bmatrix} 15-\lambda & 15-\lambda & 15-\lambda & 15-\lambda & 15-\lambda \\ 5 & 1-\lambda & 2 & 3 & 4 \\ 4 & 5 & 1-\lambda & 2 & 3 \\ 3 & 4 & 5 & 1-\lambda & 2 \\ 2 & 3 & 4 & 5 & 1-\lambda \end{bmatrix} = 0$$

$$\Rightarrow (15-\lambda) \begin{bmatrix} 1 & 1 & 1 & 1 & 1 \\ 5 & 1-\lambda & 2 & 3 & 4 \\ 4 & 5 & 1-\lambda & 2 & 3 \\ 3 & 4 & 5 & 1-\lambda & 2 \\ 2 & 3 & 4 & 5 & 1-\lambda \end{bmatrix} = 0$$

$$\Rightarrow 15-\lambda = 0$$

$$\Rightarrow \lambda = 15$$

5. Ans. A.

$$\text{Given } \gamma = (0.1 + j40)m^{-1}$$

$$\text{Here } \alpha = 0.1 \frac{\omega_p}{m}$$

We know that,

$$1 \frac{\omega_p}{m} = 8.686 \frac{dB}{m} \Rightarrow 0.1 \frac{\omega_p}{m} = 0.8686 \frac{dB}{m}$$

6. Ans. A.

Silicon atoms act as P-type dopants in Arsenic sites and n-type dopants in Gallium sites.

7. Ans. C.

$$|M| = \begin{vmatrix} 5 & 10 & 10 \\ 1 & 0 & 2 \\ 3 & 6 & 6 \end{vmatrix} = 5(0-12) - 10(6-6) = -60 - 0 + 60 = 0$$

$$\text{But a } 2 \times 2 \text{ minor, } \begin{vmatrix} 5 & 10 \\ 1 & 0 \end{vmatrix} = 0 - 10 = -10 \neq 0$$

$$\Rightarrow \text{Rank} = 2$$

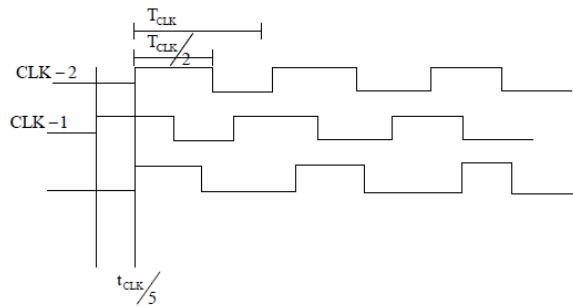
8. Ans. C.

As per the change carrier profile, base - to - emitter junction is reverse bias and base to collector junction is forward bias, so it works in Inverse active.

9. Ans. D.

Miller effect increase input capacitance, so that there will be decrease in gain in the high frequency cutoff frequency.

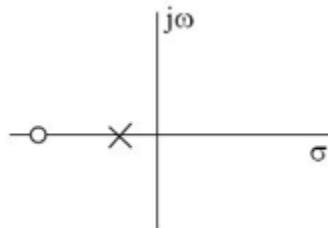
10. Ans. A.



$$\Rightarrow \text{Duty cycle of o/p} = \frac{\frac{T_{CLK}}{2} - \frac{T_{CLK}}{5}}{T_{CLK}} \times 100 = 30\%$$

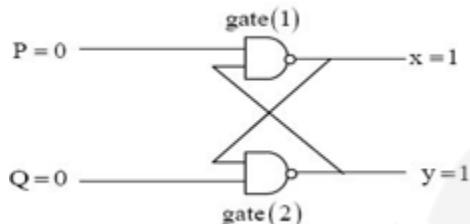
11. Ans. A.

In phase lag compensator pole is near to $j\omega$ - axis,



12. Ans. B.

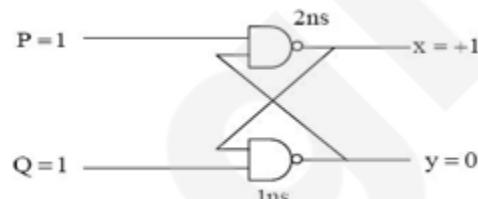
Unequal propagation delay



Case I :

Gate 1 → 2ns

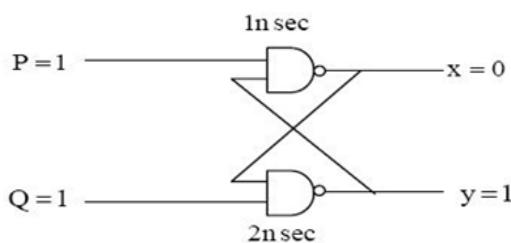
Gate 2 → 1ns



Case II :

Gate 1 → 1nsec

Gate 2 → 2nsec



∴ Either x = 1, y = 0 or x = 0, y = 1

13. Ans. A.

Required probability

$$= 6 \left(\frac{1}{6} \times \frac{1}{6} \times \frac{1}{6} \right) = \frac{1}{36} = 0.028$$

14. Ans. A.

If $x(t) = -x(-t)$ the given periodic signal is odd symmetric. For an odd symmetric signal a_n for all n

$$\text{If } x(t) = -x\left(t - \frac{\pi}{\omega_0}\right) \therefore \frac{\pi}{\omega_0} = \frac{T_0}{2} \text{ where } T_0 \text{ is}$$

fundamental period then the given condition satisfies half-wave symmetry.

For half-wave, symmetrical signal all coefficients a_n and b_n are zero for even value of n.

15. Ans. A.

$$G(s) = \frac{(s+1)}{s^p(s+2)(s+3)}$$

If p=1, e_{ss} (for ramp input) = 6

$$k_v = \frac{1}{6}$$

p=1, e_{ss} (for ramp input) = 0

$$k_p = \infty, e_{ss} = \frac{1}{1+k_p} = 0$$

16. Ans. D.

$$V_{bi} = V_T \ln \left(\frac{N_1}{N_2} \right)$$

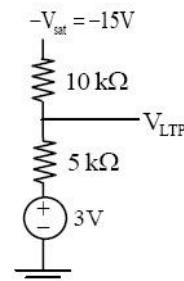
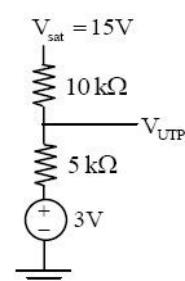
$$= 0.25 \ln \left(\frac{10^{18}}{10^{15}} \right) = 0.173V.$$

17. Ans. B.

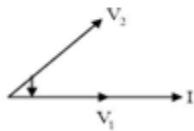
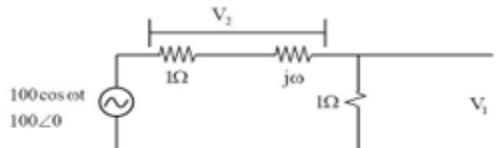
$$V_{sat} = 15V, -V_{sat} = -15V$$

$$V_{UTP} = \frac{(15-3) \times 5}{15} + 3 = \frac{12}{3} + 3 = 7V$$

$$V_{LTP} = \frac{(-15-3) \times 5}{15} + 3 = \frac{-18}{3} + 3 = -6 + 3 = -3V$$



18. Ans. A.



$$V_1 = \left(\frac{1}{2 + j\omega} \right) \times 1\omega \angle 0$$

$$V_1 = \frac{100}{\sqrt{4 + \omega^2}} \angle -\tan^{-1} \frac{\omega}{2}$$

$$V_2 = \frac{1 + j\omega}{2 + j\omega} 100 \angle 0$$

$$V_2 = \left(\frac{\sqrt{1 + \omega^2}}{\sqrt{4 + \omega^2}} \right) \times 1\omega \angle -\tan^{-1} \frac{\omega}{2} + \tan^{-1} \omega$$

$$V_2 - V_1 = \frac{\pi}{4}$$

$$-\tan^{-1} \frac{\omega}{2} + \tan^{-1} \omega + \tan^{-1} \frac{\omega}{2} = \frac{\pi}{4}$$

$$\omega = \tan \frac{\pi}{4} = 1 \text{ rad/sec}$$

19. Ans. B.

For ISI free pulse, If P(t) is having spectrum P(f)

$$\text{Then } \sum_{k=\infty}^{\infty} P(f - kR_s) = \text{constant}$$

$$R_s = 2 KSpa$$

Thin condition is met by pulse given in option B.

20. Ans. A.

$$G(s) = \frac{1}{S^{q-p}} \left[\frac{1+b_1 S^{-1} + \dots + b_p S^{-p}}{1+q_1 S^{-1} + \dots + a_p S^{-q}} \right]$$

If $S^{q-p} = S^3$, when $p=0$ and $q=3$, then

It has -60dB/dec at $\omega=\infty$

21. Ans. C.

A good trans conductance amplifier should have high input and output resistance.

22. Ans. A.

For two independent random variable

$$I(X; Y) H(X) = H(X|Y)$$

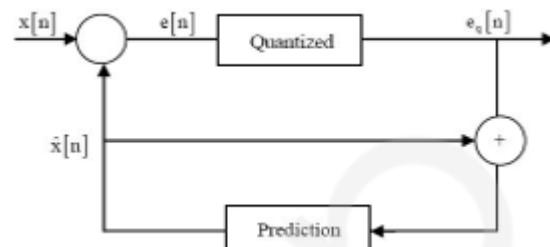
$H(X|Y) = H(X)$ for independent X and Y

$$\Rightarrow I(X; Y) = 0$$

23. Ans. D.

If a system is non-causal then a pole on right half of the s-plane can give BIBO stable system. But for a causal system to be BIBO all poles must lie on left half of the complex plane.

24. Ans. D.



DPCM Block diagram

$e_q[n]$ is quantized $e[n]$

$e[n]$ is difference of message signal sample with its prediction.

25. Ans. C.

$$C = \text{Blog}_2 \left[1 + \frac{S}{N_0 B} \right]$$

$$\text{Where } S = \frac{P_t G_t A_{er}}{4\pi r^2}$$

$$= \frac{P_t A_{er} A_e t}{\lambda^2(r^2)} = p_t \frac{4A_{er} \cdot A_e t}{4 \cdot \lambda^2(r^2)}$$

$$= \frac{P_t \cdot A_{er} \cdot A_e t}{A^2 r^2} = S$$

Channel capacity remain same.

26. Ans. A.

$$\text{Let } f(x) = x^3 + x - 1 \quad f'(x) = 3x^2 + 1$$

$$\text{Given } X_0 = 1$$

By Newton Raphson method.

1st iteration ,

$$x_1 = x_0 - \frac{f(x_0)}{f'(x_0)} = 1 - \frac{f(1)}{f'(1)} = 1 - \frac{1}{4} = \frac{3}{4} = 0.75$$

$$\text{2}^{\text{nd}} \text{ iteration. } X_2 = x_1 - \frac{f(x_1)}{f'(x_1)} = 0.75 - \frac{f(0.75)}{f'(0.75)} = \frac{0.17}{2.69} = 0.064$$

27. Ans. B.

$$u_0(t) = 5\cos(2000\pi t)$$

$$f_0 = 10 \text{ kHz}$$

$$U_1(t) = 5\cos(22000\pi t)$$

$$f_1 = 11 \text{ kHz}$$

For $u_0(t)$ and $U_1(t)$ to be orthogonal, it is necessary that

$$f_1 - f_0 = \frac{n}{2T}; (11-10) \times 10^3 = \frac{1}{2T}$$

$$\Rightarrow T = \frac{1}{2 \times 10^3} = 0.5 \text{ m sec}$$

28. Ans. A.

$$A_v = \left[\frac{V_0}{V_1} \right] = \frac{R_c}{r_e}$$

$$r_e = \frac{V_T}{I_E}$$

$$V_G = \frac{12 \times 47}{120} = 4.7 \text{ V}$$

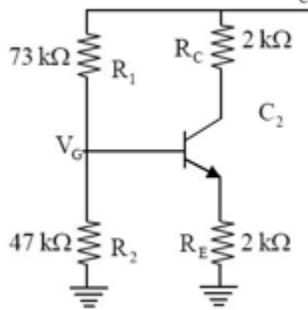
$$V_G = V_{EE} + I_E R_E$$

$$I_E = \frac{4.7 - 0.7}{2 \times 10^3} = 2 \text{ mA}$$

$$r_e = \frac{25}{2} = 12.5 \Omega$$

$$A_v = \frac{R_c \| R_L}{r_e} = \frac{2 \times 10^3 \| 8 \times 10^3}{12.5} = 128$$

$$V_{CC} = 12 \text{ V}$$



29. Ans. A.

$$V_1 = \left(\frac{4+j3}{4+j3+5-12j} \right) \times 100 \angle 0 \Rightarrow$$

$$V_1 = \left(\frac{4+j3}{9+9j} \right) \times 100 \angle 0$$

$$V_2 = \left(\frac{5-12j}{4+j3+5-12j} \right) \times 100 \angle 0 \Rightarrow \left(\frac{5-12j}{9+9j} \right) \times 100 \angle 0$$

$$\left[\frac{V_1}{V_2} \right] = \left[\frac{5-12j}{4+j3} \right] = \frac{\sqrt{5^2+12^2}}{\sqrt{4^2+3^2}} = \frac{13}{5} = 2.6$$

30. Ans. D.

$$\frac{dy}{dx} = (x+y-1)^2 \quad \dots \dots \quad (1)$$

$$\text{Put } x+y-1 = t$$

$$\Rightarrow 1 + \frac{dy}{dx} = \frac{dt}{dx}$$

$$\Rightarrow 1 + \frac{dy}{dx} = \frac{dt}{dx} - 1$$

$$\text{From (1), } \frac{dt}{dx} - 1 = t^2$$

$$\Rightarrow \frac{dt}{dx} = 1 + t^2$$

$$\Rightarrow \int \frac{1}{1+t^2} dt = \int dx$$

$$\Rightarrow \tan^{-1}(t) = x + C$$

$$\Rightarrow \tan^{-1}(x+y-1) = x + C$$

31. Ans. A.

$$G(s) = \frac{K(s^2 + 2s + 2)}{(s^2 - 3s + 2)}$$

$$C.E = 1 + G(s) = s^2 - 3s + 2 + ks^2 + 2ks + 2k = 0 \\ = s^2(1+k) + s(2k-s) + 2k + 2 = 0$$

If closed loop system to be stable all coefficients to positive $k > -1$

$$k > -1 \cap k > 1.5 \cap k > -1$$

So, $k > 1.5$

32. Ans. A.

The straight line joining A(0, 2, 1) and B(4, 1, -1) is

$$\frac{x-0}{4-0} = \frac{y-2}{1-2} = \frac{z-1}{-1-1}$$

$$\Rightarrow \frac{x}{4} = \frac{y-2}{-1} = \frac{z-1}{-2} = t \quad (\text{say})$$

$$\Rightarrow x = 4t, y = 2 - t, z = 1 - 2t$$

$$\Rightarrow dx = 4dt, dy = -dt, dz = -2dt$$

$$\Rightarrow \text{For } x = 0 \Rightarrow t = 0$$

$$\Rightarrow \text{For } x = 4 \Rightarrow t = 1$$

$$I = \int_C (2zdx + 2ydy + 2xdz)$$

$$= \int_{t=0}^1 2(1-2t)4dt + 2(2-t)(-dt) + 2(4t)(-2dt)$$

$$= \int_{t=0}^1 (-30t + 4)dt = \frac{-30t^2}{2} + 4t$$

33. Ans. A.

$$C = \frac{\epsilon A}{W}$$

$$C \propto \frac{1}{w} \text{ and } W \propto \frac{1}{\sqrt{doping}}$$

$$C \propto \sqrt{doping}$$

$$\frac{C_2}{C_1} = \sqrt{\frac{(doping)_2}{(doping)_1}} = \sqrt{\frac{10^{16}}{10^{14}}} = \sqrt{100} = 10$$

34. Ans. A.

For circular polarization, the phase difference between E_x & E_y is $\pi/2$

The phase difference for linear polarization should be π
 \Rightarrow So the wave must travel a minimum distance such that the extra phase difference of $\pi/2$ must occur.

$$\beta_y l_{\min} - \beta_x l_{\min} = \frac{\pi}{2}$$

$$\Rightarrow l_{\min}$$

$$\frac{\omega}{c} [n_y - n_x] = \pi/2 \Rightarrow \frac{2\pi l_{\min}}{\lambda_0} [n_y - n_x] = \pi/2$$

$$\Rightarrow l_{\min} =$$

$$\frac{\lambda_0}{4[n_y - n_x]} = \frac{1.5 \times 10^{-6}}{4[0.0001]} = \frac{1.5}{4} \times 10^{-2}$$

$$= 0.375 \times 10^{-2} m = 0.375 cm$$

35. Ans. A.

Given

$$x[n] = \{1, 2, 1\}; h[0] = 1$$

$$h[n] = \{1, a, b\}$$

1	2	1
1	2	1
a	a	2a
b	b	2b

$$Y[n] = \{1, 2+a, 2a+b+1, 2b+a, b\}$$

It is given that $y[1] = 3$

$$\therefore 2+a=3 \Rightarrow a=1$$

$$\text{Similarly } 2a+b+1=4 \Rightarrow b=3-2(1)=1$$

$$b=1$$

$$\therefore y[3]=2(1)+1=3$$

$$Y[4]=b=1$$

$$\therefore 10y[3]+y[4]=30+1=31$$

36. Ans. C.

$$F(s) = s^4 + s^2 + 1 = 0$$

Let take $s^2 = t$

$$t^2 + t + 1 = 0$$

$$t = \frac{-1 \pm i\sqrt{3}}{2}$$

$$\text{Where } t = s^2 = \frac{-1 \pm i\sqrt{3}}{2}$$

$$s^2 = \frac{-1+i\sqrt{3}}{2} = e^{\frac{j2\pi}{3}} \Rightarrow s^2 = \frac{-1-i\sqrt{3}}{2} = e^{\frac{-j2\pi}{3}}$$

$$S = \pm e^{\frac{j2\pi}{6}} \text{ and } s = \pm e^{\frac{-j2\pi}{6}}$$

Hence two roots contain RHS and two roots contain LHS plane.

37. Ans. A.

$$V_d = \mu_n \epsilon$$

$$\mu_n = \frac{V_d}{\epsilon} = \frac{10^7}{5 \times 10^7} 20 \frac{cm^2}{V \cdot \text{sec}}$$

$$E =$$

$$\frac{V}{d} = \frac{5}{1 \times 10^{-4}} V/cm$$

$$J_{\text{drift}} = nqV_d = nq\mu_n E$$

$$J_{\text{drift}} = nqV_a = nq\mu_n \epsilon = 10^{16} \times 1.6 \times 10^{-19} \times 20 \times 10^4 = 1.6 \text{ KA/cm}^2$$

38. Ans. A.

$$V_G = \frac{8 \times 5}{5} = 5V$$

$$V_{GS} = V_G - I_D R_s = 5 - 10^3 I_D$$

$$I_D = \frac{1}{2} \mu_n C_{\text{ox}} \left(\frac{W}{L} \right) (V_{GS} - V_T)^2$$

$$I_D = \frac{1}{2} \times 1 \times 10^{-3} (V_{GS} - V_T)^2$$

$$I_D = \frac{1}{2} \times 10^{-3} [5 - 10^3 I_D - 1]^2 = \frac{10^{-3}}{2} [4 - 10^{-3} I_D]^2$$

$$I_D = \frac{10^{-3}}{2} [16 + 10^6 I_D^2 - 8 \times 10^3]$$

$$0.5 \times 10^{-3} I_D^2 - 5I_D - 8 \times 10^{-3} = 0$$

$$I_D = 8 \text{ mA}, 2 \text{ mA}$$

I_D must be least value

$$\text{So } I_D = 2 \text{ mA}$$

39. Ans. A.

Since DC components in same in $S_x(f)$ and $S_y(f)$

$$\Rightarrow E[x(t)] = E[y(t)]$$

$$E(x^2(t)) = \text{Area under}$$

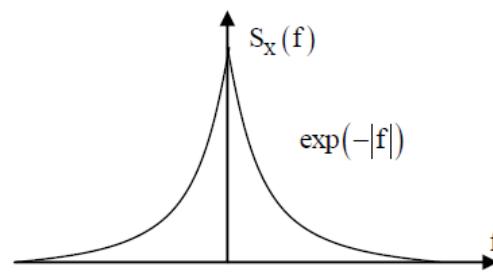
$$S_x(f) = \int_{-\infty}^{\infty} e^{-|f|} df = 2 \int_{-\infty}^{\infty} e^{-f} df = 2$$

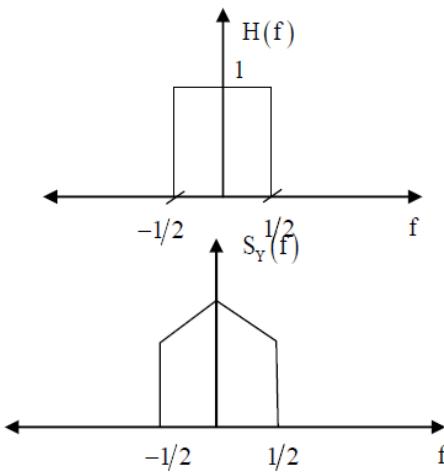
$$E(y^2(t)) = \text{Area under}$$

$$S_y(f) = \int_{-0}^{\frac{1}{2}} e^{-f} df = 2 \int_{-\infty}^{\infty} e^{-f} df = 2 \frac{e^{-f}}{-1} \Big|_{-0}^{\frac{1}{2}} = 2[1 - e^{-\frac{1}{2}}]$$

$$\Rightarrow E[x^2(t)] \neq E[y^2(t)]$$

$$\Rightarrow E[y^2(t)] \neq 2$$





40. Ans. A.

$$\Delta P = \Delta n = G_{Lo} \left(1 - \frac{L}{2} \right) \tau_p = G_{Lo} \times \tau_p = 10^{17} \times \frac{1}{2} \times 10^{-4} = \frac{1}{2} \times$$

$$10^{13} / cm^3$$

$|J_{p1} \text{ diff}| = qD_p$

$$\frac{dp}{dx} = 1.6 \times 10^{-19} \times 100 \times \frac{\frac{1}{2} \times 10^{13}}{0.1 \times 10^{-4}} = 16 A / cm^2$$

41. Ans. B.

$$G(s) = \frac{K}{(s^2 + 2s + 2)(s + 2)}$$

$$C.E = s^3 + s^2 + 76s + 4 + k = 0$$

If system to stable

$$24 > k + 4 \cap K + 4 > 0$$

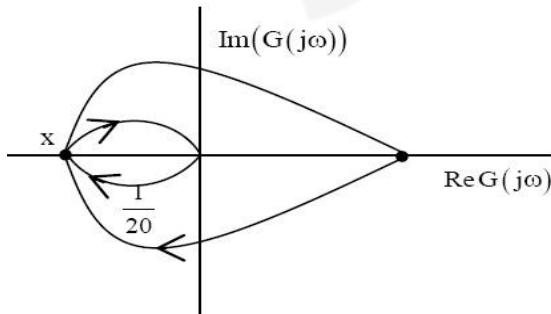
$$k > -4 \cap k < 20$$

(i) Stable condition $-4 < k < 20$ Means If $k = 10$ system stable $k = 100$ system unstable

$$\text{Or } G(j\omega) = \angle \tan^{-1} \left(\frac{\omega}{2} \right) - \tan^{-1} \left(\frac{2\omega}{2 - \omega^2} \right)$$

$$\text{If } \omega \rightarrow 0 \quad G(j\omega) = \frac{k}{4} < 0$$

$$\omega \rightarrow \infty \quad G(j\omega) = 0 \angle -270^\circ$$

So If $k = 10$ touching point = 0.5If $k = 100$ touching point = 5 $N = P - Z$, Here $P = 0$ $N = -Z$ If closed loop system to be stable, then $\Rightarrow z = 0, N = 0$,
So, $k = 0$ is stable system

42. Ans. A.

$$I_B = \frac{(2 - 0.7)}{12 \times 10^3} = 0.108 mA$$

$$I_C = \frac{(5 - 0.2)}{4.8 \times 10^3} = 1 mA$$

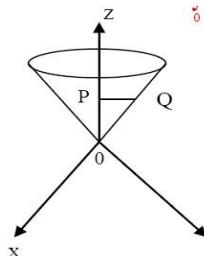
$$\beta = \frac{I_C}{I_B} = \frac{1}{0.108} = 9.259$$

$$\alpha = \frac{\beta}{1 + \beta} = \frac{9.259}{1 + 9.259} = 0.903$$

43. Ans. A.

 $PQ = \sqrt{x^2 + y^2}$ is the radius of variable circle at some Z .
 $\Rightarrow PQ^2 = x^2 + y^2 = z^3$ (Given)
∴ Volume of region revolved around z -axis =

$$\int_0^1 \pi (PQ)^2 dz = \int_0^1 \pi z^3 dz = \pi \frac{z^4}{4} \Big|_0^1 = \frac{\pi}{4} = 0.79$$



44. Ans. C.

Given the direction of propagation is

$$\hat{a}_x - \hat{a}_y$$

The orientation of \vec{E} field is $\hat{a}_x + \hat{a}_y + j2\hat{a}_z$ The dot product between above two is $= 1 - 1 + 0 = 0$ \Rightarrow It is a plane wave

We observed that

 $\bar{P} = \hat{a}_x - \hat{a}_y, \hat{a}_x + \hat{a}_y \text{ and } j2\hat{a}_z$ are normal to each other.So electric field can be resolved into two normal component along $\hat{a}_x + \hat{a}_y$ and $j2\hat{a}_x$ The magnitude are $\sqrt{2}$ and 2 and $\theta = \frac{\pi}{2}$

So elliptical polarization.

45. Ans. D.

In given diagram

Prsent State	D _A	D _B	X _m	X _n	X _m =0 Next State		X _m =1 Next State	
					θ _A ⁺	θ _B ⁺	θ _A ⁺	θ _B ⁺
00	0	1	0	1	0	1	0	1
01	1	1	0	1	1	1	1	1
11	0	1	0	1	0	1	0	0
01	1	1	0	1	1	1	0	1

When X_m=0 2 State

When X_m=1 3 State

46. Ans. B.

Fourier series coefficient a_k is unaffected by scaling operating. Thus (I) is true and (II) is false. T= 1sec for x(t) and if it compressed by '3' then the resultant period

$$T = \frac{1}{3}$$

$$\therefore \text{Fundamental frequency} = \frac{2\pi}{T_1} = 6\pi \text{ rad/sec.}$$

Thus (III) is correct.

47. Ans. A.

CLK	A B C D				
	D _m = A ⊕ B	A → B	B → C	C → D	
0	1	1	0	1	→ initial state
1	0	1	1	0	
2	0	0	1	1	
3	1	0	0	1	
4	0	1	0	0	
5	0	0	1	0	
6	0	0	0	1	
7	1	0	0	0	
8	1	1	0	0	
9	1	1	1	0	
10	1	1	1	1	→ Final state

10 clock pulse required.

48. Ans. C.

We have series of f(x) around x=0 is f(x)=

$$f(0) + xf'(0) + \frac{x^2}{2!} f''(0) + \frac{x^3}{3!} f'''(0)$$

(upto powers of "x" less than or equal to "3")

Given

$$f(x) = e^{x+x^2} \Rightarrow f(0) = 1$$

$$f'(x) = e^{x+x^2}(1+2x) \Rightarrow f'(0) = 1$$

$$f''(x) = e^{x+x^2}(1+2x) + 2e^{x+x^2} \Rightarrow f''(0) = 3$$

$$f'''(x) = e^{x+x^2}(1+2x)^3 + e^{x+x^2} 4(1+2x) + 2(1+2x)e^{x+x^2}$$

$$\Rightarrow f'''(0) = 7$$

$$\therefore f(x) = e^{x+x^2}$$

$$= 1 + x + \frac{x^2}{2!}(3) + \frac{x^3}{3!}(7) = 1 + x + \frac{3}{2}x^2 + \frac{7}{6}x^3$$

49. Ans. B.

MVI A, 33H A ← 33H

MVI B, 78H B ← 78H

ADD B B ← ABH

CMA A ← 54H

ANI 32H A ← 10H

A → 0011 0011 A → 1010 1011

B → 0111 1000 B → 0101 0100

1010 1011

0101 0100

0011 0010

0001 0000

50. Ans. A.

Under dc condition inductor acts as short all

$$\therefore I_{\text{total}} = \frac{15}{1} = 15A$$

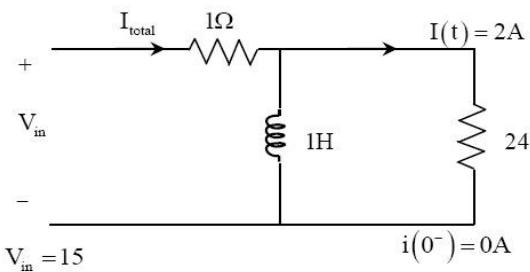
$$i(t) = (i(0^-) - i(\infty))e^{-\frac{t}{2}} + i(\infty) \quad i(0^-) = i(0^+) = 0A$$

$$i(t) = (0 - 15)e^{-\frac{3}{2}t} + 15$$

$$I_{\text{total}} =$$

$$\frac{I_{\text{total}}}{3} = \frac{15}{3}(1 - e^{-\frac{3}{2}t})$$

$$2 = 5 \left(1 - e^{-\frac{3}{2}t} \right) \Rightarrow t = 0.34 \text{ sec}$$



51. Ans. A.

The null occurs along axis of the antenna which is \$\theta=90^\circ\$, \$\phi=45^\circ\$

52. Ans. A.

Given Amplifier is using -ve feed back

$$A_f = \frac{A_0}{1 + A_0\beta}$$

$$\beta = \frac{1}{80}; A_0 = 10^5$$

$$A_f = \frac{10^5}{1+10^5/8} = 79.93$$

$$f_{cut} = 8Hz \times (1 + A_0 \beta) = 10008Hz$$

$$A_f(\omega) = \frac{A_f}{\sqrt{1+(f/f_{cut})^2}}$$

$$= \frac{79.93}{\sqrt{1+\left(\frac{15 \times 10^3}{10008}\right)^2}} \\ = 44.3$$

53. Ans. A.

It is given that,

$$H[0] = \frac{1}{3}; H[1] = \frac{1}{3}; H[2] = \frac{1}{3} \text{ &}$$

$H[n] = 0$ for $n < 0$ and $n > 2$.

$$\therefore h[n] = h[0]\delta[n] + h[1]\delta[n-1] + h[2]\delta[n-2] \\ = \frac{1}{3}[\delta[n] + \delta[n-1] + \delta[n-2]]$$

Apply DTFT on both sides,

$$\therefore H(\omega) = \frac{1}{3}[1 + e^{-j\omega} + e^{-2j\omega}]$$

Given that $H(\omega_0) = 0$ & $0 < \omega_0 < \pi$

$$\Rightarrow H(\omega_0) = 0 \text{ & } 0 < \omega_0 < \pi$$

$$\Rightarrow H(\omega_0) = \frac{1}{3} \left[1 + e^{\frac{-3j\omega_0}{2}} \left(e^{\frac{-j\omega_0}{2}} + e^{\frac{j\omega_0}{2}} \right) \right] = 0$$

$$\therefore 1 + 2e^{-3j\omega_0} \cos \frac{\omega_0}{2} = 0$$

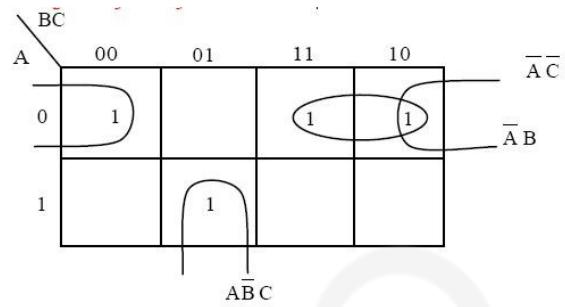
$$\text{Consider } |H(\omega_0)| \Rightarrow \cos \frac{\omega_0}{2} = \frac{1}{2}$$

$$\therefore \omega_0 = \frac{2\pi}{3}$$

$$\omega_0 = 2.094$$

54. Ans. B.

$$F = M_0 + M_1 + M_2 + M_3 + M_5 \rightarrow \min term$$



55. Ans. A.

$$\text{Given: } (t) = \begin{cases} \frac{2 \sin(300\pi t)}{\pi t} & t \neq 0 \\ 600 & t = 0 \end{cases}$$

$$\text{Thus } h(t) = 600 \sin c(300t)$$

$$\therefore H(f) = 2 \text{rect}\left(\frac{f}{300}\right)$$

$$\text{Given } x(t) = 4 \cos 200\pi t + 800 \cos 400\pi t$$

In f-domain

$$X(f) = 2[\delta(f-100) + \delta(f+100)] + 4[\delta(f-200) + \delta(f+200)]$$

