1. Ans. A.

Before superlative article 'the' has to be used. 'one of' the expression should take plural noun and so option 'C' and 'D' can't be the answer.

2. Ans. B. 'lose' is verb.

3. Ans. A.

'effectiveness' is noun and 'prescribed' is verb. These words are apt and befitting with the word 'medicine.'

4. Ans. A.



5. Ans. C.



6. Ans. C.



P (a person infected but does not show symptoms) = $0.50 \times 0.70 = 0.35$ The percentage is 35%

7. Ans. B.

The words 'was confident that they would reciprocate' and 'last week proved him wrong' lead to statements iii and iv as logically valid inferences.

8. Ans. D.

From given data, the following arrangement is possible Shiva Leela Pavithra Among four alternatives, option D is TRUE.

9. Ans. C.

$$q^{-a} = \frac{1}{r}, r^{-b} = \frac{1}{s}, s^{-c} = \frac{1}{q}$$

$$q^{a} = r, r^{b} = s, s^{c} = q$$

$$r = q^{a} = (s^{c})^{a} = s^{ac}$$

$$s = r^{b} = (s^{ac})^{b} = s^{abc} \Rightarrow abc = 1$$
10. Ans. C.
Q's one hour work = $\frac{1}{25 \times 12}$
R's one hour work = $\frac{1}{50 \times 12}$
Since Q has taken 2 days sick leave, he has worked only
5 days on the end of seventh day.
Work completed by Q on 7th day= (5×12) $\frac{1}{25 \times 12}$
Work completed by R on 7th day= (5×12) $\frac{1}{50 \times 12}$
Ratio of their work

$$= \frac{5 \times 12}{25 \times 12} / \frac{7 \times 12}{50 \times 12} \Rightarrow 20:21$$
11. Ans. C.
 $M.M^{4k+1} = M^{4K}.M^{2} (M^{4})^{k}.M^{2} = I.M^{2} = M^{2}$
 $A is not correct$
 $M.M^{4k+2} = M^{4K}.M^{4} (M^{4})^{k}.M^{4} = I.I = I$
 $C is correct$
 $M.M^{4k} = M.(M^{4})^{k} = M(I) = M$.
 $D is not correct$
12. Ans. A.
We know that if X is parameter of poison's distribution
 $Then, First moment = \lambda$
Score d moment $= \lambda^{2}$

aradeup

Second moment $= \lambda^2 + \lambda$ *Given that* $\lambda^2 + \lambda = 2$ $\Rightarrow \lambda^2 + \lambda - 2 = 0$ $(\lambda+2)(\lambda-1)=0$ $\lambda = -2 \ or \ 1$ $(\lambda \neq -2)$ $\lambda = 1$ \therefore First moment = 1

5

=

13. Ans. B.

We know that every differentiable function is continuous but converse need not be true

14. Ans. A.

15. Ans. C.

Since the integration of an odd function is even in this logic A and B cannot be the answer as they are odd functions.

However both C and D are even functions but the integration of a linear curve has to be parabolic in nature and it cannot be a constant function. Based on this Option C is correct.

16. Ans. C.

If the input to a system is its eigen signal, the response has the same form as the eigen signal

17. Ans. B.

Consider x (t) = $cos(w_0 t)$

If x (t) is sampled with a sampling period

$$T_{s}, x[n] = \cos\Omega_{0}n \text{ is obtained}$$

Here, $\frac{\Omega_{0}}{T_{s}} = \omega_{0}$
 $\frac{2\pi m}{N_{0}T_{s}} = \frac{2\pi}{T_{0}}$
 $\therefore \frac{T_{0}}{T_{s}} = \frac{N_{0}}{m}$ Which must be a rational number
Thus, $\frac{T}{T_{s}} = \frac{12}{10} = \frac{6}{5}$ lives a periodic signal after sampling.

18. Ans. B. $a^{n}u[n]; ROC : |z| > |a| = R_{1}$ $b^{n}u[n]; ROC : |z| > |b| = R_{2}$ $a^{n}u[n] + bnu[n]; ROC : R_{1} \cap R_{2} = |z| > |b|$

19. Ans. D. A two port network is reciprocal in transmission parameters if AD - BC = 1 i.e. Determinant(T) = 1

20. Ans. A. Sinusoidal signal frequency = 33 Impulse train frequency = 46 Resultant signal contains spectral frequencies ± 33 , ± 13 , ± 7.9 , ± 59 etc, Thus if it is passed through ideal LPF of cutoff frequency 23Hz only ± 13 Hz frequency is filtered out. Output signal fundamental frequency = 13 Hz.

21. Ans. A.

New energy level is near to conduction band, so it is pentavalent atoms to form n-type semiconductor.

22. Ans. C.

$$\rightarrow I \propto \frac{1}{L} soL \downarrow I_{OFF} \uparrow$$

$$\rightarrow r_{d} = \frac{\partial V_{DS}}{\Pi_{D}} = \frac{L}{\mu_{n}c_{ox}W(V_{us} - V_{t} - V_{DS})}$$

$$soL \downarrow I_{OV} \downarrow$$

 $\rightarrow\,$ If the channel length reduces, then threshold voltage also changes

aradeur

$$\rightarrow L \downarrow I_{ON} \downarrow$$

So option C. is matching.

23. Ans. B.

Voltage at (+) terminal $V_{+} = V_{CC} - V_{ref}$

Voltage at emitter of PNP BJT $V_E = V_{CC} - V_{ref}$

The current I_{E} through R

$$I_E = \frac{V_{CC} - (V_{CC} - V_{ref})}{R}$$

$$I_E = \frac{V_{ref}}{R}$$

$$I_C = I_0$$

$$I_C = \alpha I_E = (\frac{\beta}{\beta + 1})I_E \Longrightarrow \boxed{I_C = I_0(\frac{\beta}{\beta + 1})}$$

24. Ans. A.

The voltage at (-) terminated of the OP-Amp

$$V_{(-)} = \frac{2}{2+8} \times 10 = 2V$$

The output of the op-Amp goes to +V_{cc} whenever $V_i > V_{(-)}i.e$ $V_i > 2V$ makes BJT turn ON. So, the LED glows. The sections of the wave form become more than 2V for the range [a to b, (c to d) and (e to f)] So LED

25. Ans. A.

glows 3 times.

Sol. When the output voltage is positive the diode D_i is turned on making $100k\Omega$ resistor to become parallel to $22.1k\Omega$. So the gain is reduced. When the output voltage becomes negative the diode D₂ is turned on thereby again $100k\Omega$ resistor to become parallel to $22.1k\Omega$. So the gain is reduced. With the use of diodes, the non-ideal OP-Amp is made stable to produce steady









$$x = \sum m(7)$$

$$y = \sum m(3,6)$$

$$z = \sum m(3,6,7)$$

$$= \overline{ABC} + AB\overline{C} + ABC$$

$$= \overline{ABC} + AB$$

$$= B(\overline{AC} + B)$$

$$= B(A+c)$$

The transfer characteristics of the CMOS inverter is as follows



Since the inverter is connected in feedback loop formed by connecting 1OXQ resistor between the output and input, the output goes and stays at the middle of the characteristics

 $V_a = \frac{V_{IR} + V_{IH}}{2}$





$$I = P - Z$$

For closed loop stability Z = 0, N = P \therefore (-1, j0) should be encircled in Counter clock wise direction equaling P poles in RHP.

31. Ans. B.

$$R_b = 56 \text{ kbps}, \alpha = 0.25$$

 $BW = \frac{R_b}{2} [1 + \alpha] = \frac{56}{2} [1 + 0.25] \text{kHz} = 35 \text{ kHz}$

33. Ans. B.

$$s(t) = 5 \cos 1600\pi t$$

$$+20 \cos 1800\pi t + 5\cos 2000\pi t$$

$$= A_{c}[1 + \frac{A_{m}}{A_{c}}\cos 200\pi t]\cos(1800\pi t)$$

$$A_{c} = 20$$

$$\frac{A_{c}\mu}{2} = 5 \Longrightarrow \mu = \frac{5 \times 2}{20} = 0.5$$

$$\mu = 0.5$$

34. Ans. A.

Consider a Gaussian surface a sphere of radius 10m

To ensure $\nu - \sigma$ at radius 10m, the total charge enclosed by Gaussian surface is zero

$$Q_{enc} = 0$$

20 × 2² - 4 × 4² = P_s × 8² = 0
 $\Rightarrow P_s = -0.25nc / m^2$

35. Ans. B.
Given
Propagation contact,
$$P = (2 + j5) \text{ m}^{-1}$$
,
characteristic impedance $z_0 = 50 \Omega$,
angular frequency $\omega = 10^6 \text{ rad/sec}$,
 $P = \sqrt{(R + j\omega L)(G + j\omega C)}$
 $z_0 = \sqrt{\frac{(R + j\omega L)}{(G + j\omega C)}}$
 $p_{z_0} = R + j\omega L$
 $\Rightarrow R + j\omega L = (100 + j250)$
 $\therefore R = 100 \Omega/m$
 $L = \frac{250}{10^6} = 250 \mu H/m$
 $\frac{P}{z_0} = G + j\omega C$
 $G + j\omega C = \left(\frac{2}{50} + j\frac{5}{50}\right)$

2

:. G = 0.04 s/m
C =
$$\frac{5}{50 \times 10^6} = 0.1$$

 $C = \frac{5}{50 \times 10^6} = 0.1 \mu F/m$ Therefore line constants L, C, R & G are respectively L = 250 µH/m, C = 0.1 µF/m, R = 100 Ω/m, G = 0.04 s/m

36. Ans. B. Method-I:-

$$= \frac{1}{2\pi} \int_{x=-2}^{2} \int_{y=-\sqrt{4-x^{2}}}^{\sqrt{4-x^{2}}} (x+y+10) dx dy$$

$$= \frac{1}{2\pi} \int_{-2}^{2} \left[2 \int_{0}^{\sqrt{4-x^{2}}} (x+10) + 0 \right] dx$$

$$= \frac{1}{2\pi} \int_{-2}^{2} (x+10)(y)_{0}^{\sqrt{4-x^{2}}} dx$$

$$= \frac{1}{\pi} \int_{-2}^{2} (x\sqrt{4-x^{2}} + 10\sqrt{4-x^{2}} dx)$$

$$= \frac{1}{\pi} \left[0 + 10 \times 2 \int_{-2}^{2} \sqrt{4-x^{2}} dx \right]$$

$$= \frac{20}{\pi} \left[\frac{x}{2} \sqrt{4-x^{2}} + \frac{4}{2} \sin^{-1} \left(\frac{x}{2} \right) \right]_{0}^{2}$$

$$= \frac{20}{\pi} \left[0 + 2 \left(\frac{\pi}{2} \right) \right] = 20$$
Method – II:-

gradeup

$$\frac{1}{2\pi} \iint_{D} (x + y + 10) dx dy$$

$$= \frac{1}{2\pi} \int_{-0}^{2} \int_{0}^{2\pi} [r(\cos \theta + \sin \theta) + 10] r dr d\theta$$
(Changing into polar coordinates by $x = r\cos\theta$)
37. Ans. A.

$$\begin{bmatrix} x(n) \\ x(n-1) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix}^{n} \begin{bmatrix} 1 \\ 0 \end{bmatrix} n \ge 2$$

$$n = 2$$

$$\begin{bmatrix} x(2) \\ x(1) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix}^{2} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 2 & 1 \\ 1 & 1 \end{bmatrix}^{0} \begin{bmatrix} 2 \\ 2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 2 \\ 2 \end{bmatrix}$$

$$x(2) = 2, x(1) = 1$$

$$n = 3$$

$$\begin{bmatrix} x(3) \\ x(2) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & 0 \end{bmatrix}^{3} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 3 & 2 \\ 2 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 3 \\ 2 \end{bmatrix}$$

$$x(3) = 3, x(2) = 2$$
From the above values we can write the recursive relation as
$$x(n) = x(n-1) + x(n-2)$$

$$x(2) = x(1) + x(0) = 1 + 1 = 2$$

$$x(3) = x(2) + x(1) = 2 + 1 = 3$$

$$x(4) = x(3) + x(2) = 3 + 2 = 5$$

$$x(5) = x(4) + x(3) = 5 + 3 = 8$$

$$x(6) = x(5) + x(4) = 8 + 5 = 13$$

$$x(7) = x(6) + x(5) = 13 + 8 = 21$$

$$x(8) = x(7) + x(6) = 21 + 13 = 34$$

$$x(9) = x(8) + x(7) = 34 + 21 = 55$$

$$x(10) = x(9) + x(8) = 55 + 34 = 89$$

$$x(11) = 89 + 55 = 144$$

$$x(12) = 144 + 89 = 233$$
38. Ans. A.

$$-\frac{1}{2\pi} \oint_{c} \frac{\sin z}{(z - 2\pi j)^{3}} dz = -\frac{1}{2\pi} \times 2\pi j \times \frac{f'' 2\pi j}{2!}$$
(by Cauchy integral formula)
$$f(z) = \sin z$$

$$f''(z) = -\sin z$$

$$-\frac{1}{2\pi} \oint_{c} \frac{\sin z}{(z - 2\pi j)^{3}} dz = -\frac{1}{2\pi} x 2\pi j \times \frac{f'' 2\pi j}{2} = -\frac{1}{2\pi} x 2\pi j \times \left(\frac{-\sin 2\pi j}{2}\right) = -\frac{1}{2} \sinh 2\pi$$

$$= -133.87$$



39. Ans. A.
Volume=
$$\int_{3}^{5} \int_{\pi/8}^{\pi/4} \int_{3}^{4.5} \rho d\rho d\phi dz = 4.71$$

40. Ans. B. Sol. Laplace transition of one cycle of

$$f(t) = \frac{1}{S} \left[1 - e^{-s_r/2} \right]$$

 \therefore Laplace transition of causal periodic square wave given in f(t) is,

$$F(s) = \frac{\frac{1}{s} \left[1 - e^{-ST/2} \right]}{(1 - e^{-ST})}$$
$$= \frac{\frac{1}{s} \left[1 - e^{-ST/2} \right]}{\left[1 - e^{-ST/2} \right] \left[1 + e^{-ST/2} \right]} = \frac{1}{s \left[1 + e^{-ST/2} \right]}$$

41. Ans. A.

The property of any LTI system or network is if the excitation contains 'n' number of different frequency then the response also contains exactly n number of different frequency term and the output frequency and input frequency must be same however depending on components there is a possible change in amplitude and phase but never the frequency.

ightarrow If the source has 3 frequency terms as given

$$\sum_{k=1}^{3} a_{k} \cos k\omega_{0}t$$

$$b_{k} \text{ and } \phi_{k}t \geq 01 - e^{-t/T}$$

$$t - T\left(1 - e^{-t/T}\right)$$

$$Y(s) = \frac{K}{s^{2}(1 + s^{2})} = \frac{K_{1}}{s} + \frac{K_{2}}{s^{2}} + \frac{K_{3}}{1 + s\tau}$$

$$Y(t) = K_{1}u(t) + K_{2}u(t) + K_{3}e^{-t/2}$$

$$\to X - R$$

$$Y - P$$

$$Z - Q$$

$$\left(1 - e^{-t/\tau}\right)X(s) = \frac{k}{1 + s\tau}$$

 \Rightarrow y(t) = ke^{-t/\tau}

then any voltage or any current of any element should have also 3 terms based on this option B. and D. are eliminated.

 \rightarrow If we take option C.. It has 3 frequency term but it also suggest there is a phase change so 4, but amplitude must be same as input as ak is present which may not be true always.

 \rightarrow So option A. is correct, as it suggest frequency term of output and inputs are same with possible change in amplitude and phase, because we have (b_k and ϕ_k).

42. Ans. C.

 \rightarrow In general the first order, L.P.F filter transfer function

is $G(s) = \frac{k}{1+s\tau}$ because G(0) = k and G (co) = 00, if we take this transfer function as reference and give different input such as s(t).r(t).u(t) \rightarrow if input is s(t)

$$Y(s) = \frac{k}{1+s\tau} X(s) = \frac{k}{1+s\tau} 1$$

$$\Rightarrow y(t) = ke^{-t/\tau}$$

$$\Rightarrow \text{ if input is u(t)}$$

$$Y(s) = \frac{k}{1+s\tau} = K_1 \left(1-e^{-t/\tau}\right)$$

$$\Rightarrow \text{ if input is r(t)}$$

$$Y(s) = \frac{K}{s^2(1+s^2)} = \frac{K_1}{s} + \frac{K_2}{s^2} + \frac{K_3}{1+s\tau}$$

$$Y(t) = K_1 u(t) + K_2 u(t) + K_3 e^{-t/2}$$

$$\Rightarrow X - R$$

$$Y - P$$

$$Z-Q$$

43. Ans. A.



44. Ans. C.

To find maximum power transferred to load we need to obtain Thevenin equivalent of the circuit



$$V_0 = \frac{2}{3+2}5 = 2V$$
$$V_{0C} = \frac{40}{10+40}100V_0 = \frac{4}{5} \times 100 \times 2 = 160V$$

 \rightarrow Obtaining I_{SC}



$$I_{SC} = \frac{1}{2} = \frac{1}{10} = 20 mA$$
$$\rightarrow R_m = \frac{V_{0C}}{I_{SC}} = \frac{160}{20} = 8k\Omega$$

 \rightarrow So the network is



→ For MPTR = 8k

$$P_{mcr} = \frac{V_{+n}^2}{4R_{+n}} = \frac{160^2}{(4 \times 8) \times 103} = 0.8 watt.$$

45. Ans. A. Consider

$$\frac{1}{\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) \sin^{2}(2\omega) d\omega$$

= $\frac{1}{\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) \left(\frac{1-\cos 4\omega}{2}\right) d\omega$
= $\frac{1}{\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) \sin^{2} d\omega - \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) \cos 4\omega d\omega$
 $\frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) \cos 4\omega d\omega = 0$ For the given x[n]
 $\therefore \frac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) d\omega = x[0]$
 $\frac{1}{\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) \sin^{2} 2\omega d\omega = 8$





47. Ans. A.
IDs =

$$I_{DS} = \frac{1}{2} \mu_N C_{OX} \frac{W}{L} (V_{GS} - V_T)^2 (1 + \lambda V_{DS})$$

 $g_{dS} = \frac{dI_{DS}}{dV_{DS}} = \lambda \frac{1}{2} \mu_N C_O \times \frac{W}{L} (V_{GS} - V_T)^2$
 $= 0.09 \times 0.5 \times 70 \times 10^{-6} \times 4 (1.8 - 0.3)^2$
 $= 28.476 \, \mu s$

48. Ans. B.





49. Ans. A.

$$P_{n0} = \frac{n_i^2}{N^D} = \frac{2.25 \times 10^{20}}{5 \times 10^{16}} = 0.5 \times 10^4 / cc$$

$$\rightarrow \Delta P = G\tau_{p0} = 1.5 \times 10^{20} \times 10^{-6} \times 0.1$$

$$= 1.5 \times 10^3 / cc$$

$$\Delta P(t) = \Delta P e^{-t/\tau_p}$$

$$P(t) = \Delta P(t) + P_{n0} \approx \Delta P(t)$$

$$\Delta P(0) = \Delta P = 1.5 \times 10^3 / cc$$

$$\Delta P(t = 3) = 7.47 \times 10^{11} / cc$$

50. Ans. A.



$$\therefore V_0 = (V_{P1} + V_{P2} + \dots + V_{Pn}) - (V_{N1} + V_{N2} + \dots + V_{Nn})$$

If the series approaches ∞ then

 $V_0 = \left(1 + \frac{1}{3} + \frac{1}{5} + \frac{1}{7} \dots \right) - \left(\frac{-1}{2} + \frac{1}{4} + \frac{1}{6} - \dots \right)$ $= 1 + \frac{1}{2} + \frac{1}{3} + \frac{1}{4} + \frac{1}{5} + \dots$ $= \infty$

This series is called harmonic series which is a divergent infinite series $\therefore V_0 = +\infty = + V_{sat} = + V_{CC} = +15V$

51. Ans. D.

The photo diode with Responsivity 0.8A/W \therefore Diode current = 0.8A/W[10µW] = 8 × 10⁻⁶A V₀ = -8µ (1M) = -8V



Therefore the value of photo current throughput the load is $-800 \ \mu A$

52. Ans. A.

As we know in a decoder w.r.t any binary input combination the corresponding output pin is high and remaining low.

 \rightarrow Similarly to the encoder one input is high among all and its equivalent binary combination is available at output.

 \rightarrow In this case to identify the functionality, let give some arbitrary binary input and observe the output.

 \rightarrow Let [X₂ X₁ X₀] is [1 0 1] respectively then OP₅ = 1 = IP? Then [Y₂ Y₁ Y₀] is [1 0 1]

If $[X_2 X_1 X_0]$ is $[1 \ 1 \ 1]$ then $[OP_7 = IP_5 = 1]$ so $[Y_2 Y_1 Y_0 = 101] [X_2 X_1 X_0]$ is $[1 \ 0 \ 0]$ then $[OP_4 = IP_6 = 1]$ so $[Y_2 Y_1 Y_0 = 110]$

 \rightarrow From the above we can say that If input 101 then output is 101 101 101 110 110 So input binary and output gray.

53. Ans. B.

Decoder inputs will behaves as MUX select lines and when the output of decoder is high then only corresponding buffer will be enable and passed the inputs (P,Q,R,S) to the output line, so it will work as 4-to-1 multiplexer.

54. Ans. C.

In push operation 3 cycles involved: 6T+3T+3T = 127POP operation 3 cycles involved: 4T+3T+3T = 107So in the opcode fetch cycle 2T states are extra in case of push compared to POP and this is needed to decrement the SP.

55. Ans. B.

Sol. In this first we need to find the break point by finding the root of $\frac{dk}{ds} = 0$ and then by using magnitude condition value of k can be obtained.

$$G(s) = \frac{K}{s^2 + 5s + 5}$$

$$k = -(s^2 + 5s + 5)$$

$$\frac{dk}{ds} = 0$$

$$\Rightarrow 2s + 5 = 0 \Rightarrow s = -2.5$$



Applying magnitude condition |G(s)| = 1

$$\left|\frac{K}{s^2 + 5s + 5}\right|_{s=-2.5} = 1$$
$$\Rightarrow \left[\frac{k}{(-2.5^2) + [5x(-2.5)] + 5}\right] = 1$$
$$\Rightarrow \left[\frac{k}{6.25 - 12.5 + 5}\right] = 1$$
$$\Rightarrow \left|\frac{k}{-1.25}\right| = 1 \Rightarrow k = 1.25$$

56. Ans. A. K = 2.86 Peak over shoot 10%

$$\Rightarrow e^{\frac{-\pi\xi}{\sqrt{1-\xi^2}}} = 0.1$$
$$\Rightarrow \left[\frac{-\pi\xi}{\sqrt{1-\xi^2}}\right]^2 = [In0.1]^2$$
$$\Rightarrow \frac{-\pi\xi}{\sqrt{1-\xi^2}} = \left[\frac{\pi}{In0.1}\right]^2$$
$$\Rightarrow \frac{1}{\xi^2} = 1 + \left[\frac{\pi}{In0.1}\right]^2$$
$$\Rightarrow \frac{1}{\xi^2} = 2.86$$
$$\Rightarrow \xi^2 = \frac{1}{2.86} = 0.34$$
$$\Rightarrow \xi = 0.59$$

→ The characteristic equation of above transfer function is $s^2 + 2s + k = 0$ Comparing with standard equation $s^2 + 2\xi\omega_n + {\omega_n}^2 = 0$ $\Rightarrow 2\xi\sqrt{k} = 2$ $\Rightarrow \sqrt{k} = \frac{2}{2}$

$$\Rightarrow k = \left[\frac{2}{2\xi}\right]^2 = \frac{1}{\xi^2} = 2.86$$

$$k = 2.86$$

57. Ans. A.

We can proceed here by taking this polynomial as characteristic equation and conclusion can be draw by using RH criterion. As we are interested to know how many roots are lying on right half of s plane.

S ⁴	2	0	-2
	-5	+5	0
s	4	-2 0	$\begin{cases} Since row of zero \\ occurs the \\ auxiliary equation \\ is \\ A.\varepsilon: 2s^2 - 2 \\ \frac{d}{ds}(At) = 4 \end{cases}$

 \rightarrow The number of roots i.e. the number of zeros in this case in right half of plane is number of sign changes \rightarrow Number of sign changes = 3

```
58. Ans. A.
```

$$\sum_{i=1}^{\infty} \left(\frac{1}{2}\right)^{i} \log_{2}(2)^{i} = \sum_{i=1}^{\infty} \left(\frac{1}{2}\right)^{i} \log_{2}^{2}$$
$$= \sum_{i=1}^{\infty} i \left(\frac{1}{2}\right)^{i}$$
$$= \sum_{i=1}^{\infty} i a^{i-1+1} = a \sum_{i=1}^{\infty} i a^{i-1} = a \sum_{i=1}^{\infty} \frac{d}{da} (a^{i})$$
$$= a \frac{d}{da} \left[\sum_{i=1}^{\infty} a^{i}\right] = \frac{a}{(1-a)^{2}} = \frac{1/2}{1/4} = 2bits$$

59. Ans. A. Cross over Probability P= 0.1 X = number of errors $\frac{1}{2}P(x \ge 2|_{000sent}) + \frac{1}{2}P(x \ge 2|_{111sent})$ $= 2 \times \frac{1}{2} \left[\left(\frac{3}{2} \right) (0.1)^2 (0.9)^1 + \left(\frac{3}{2} \right) (0.1)^3 (0.9)^0 \right]$ $= 3(0.01)(0.9) + (0.3)^1 = \frac{27}{1000} + \frac{1}{1000} = \frac{28}{1000}$ = 0.028

60. Ans. A.

$$r(t) = S(t) + n(t)$$

$$r_{s}(t) = \int_{0}^{t} s(u)h(t-u)du$$

$$r_{n}(t) = \int_{0}^{t} n(u)h(t-u)du$$

$$SNR = \frac{Y_{s}^{2}(t)}{E[Y_{s}^{2}(t)]} = \frac{\left[\int_{0}^{t} s(u)h(t-u)du\right]^{2}}{\frac{N_{0}}{2}\int_{0}^{t} h^{2}(t-u)du}$$

By CS in equality (ifh(t-u) = CS(u))

$$SNR_{opt} = \frac{\int_{0}^{b} s^{2}(u) du}{\frac{N_{0}}{2}} = \frac{2E_{s}}{N_{o}}$$
$$SNR_{opt} = \frac{2E_{s}}{N_{o}} \text{ if } E_{n} \ge E_{s}$$

61. Ans. D.

Current density, $= 400 \sin \theta = 222$

$$\vec{J} = \frac{400\sin\theta}{2\pi(r^2 + 4)} \vec{a}_r A/m^2$$

current passing through the portion of sphere of radius r = 0.8 m is given by $I = \int \vec{J}.d\vec{s} (r = constant)$

$$d\vec{s} = r^{2} \sin \theta \, d\theta \, d\phi \, \hat{a}r \, d \, (\because r = 0.8 \text{ m})$$

$$I = \int_{\theta = \frac{\pi}{2}}^{\frac{\pi}{4}} \int_{\theta = 0}^{2\pi} \frac{400 \sin \theta}{2\pi (r^{2} + 4)} r^{2} \sin \theta \, d\theta \, d\phi$$

$$= \frac{400(0.8)^{2}}{2\pi (0.8^{2} + 4)} \left[\left(\frac{\pi}{4} - \frac{\pi}{12}\right) - \left(\sin\left(\frac{\pi}{2}\right) - \sin\left(\frac{\pi}{6}\right)\right) \right] \times (2\pi)$$

$$\therefore I = 7.45 \text{ Amp}$$

The average current density through the given sphere surface is

$$J = \frac{1}{\text{Area of } r = 0.8\text{m sphere}}$$
$$= \frac{7.45}{(0.8)^2 \int_{\theta=\pi/2}^{\pi/4} \int_{\phi=0}^{2\pi} \sin \theta \, d\theta \, d\phi}$$
$$= \frac{7.45}{1.04}$$
$$\therefore J = 7.15 \text{ A/m}^2$$

T





63. Ans. A. Given Lossless horn antennas $\eta T = \eta R = 1$ Power Gain = Directivity Directivity of Txing antenna, $D_T = 18$ dB 10 log $D_T = 18$ G_T (or) $D_T = 63.09$ Directivity of Rxing antenna, $D_R = 22$ dB $10 \log D_R = 22$ G_R (or) $D_R = 158.48$ input power $P_{in} = 2$ W Spacing, $r = 200 \lambda$



Friis transmission formula in given by

$$P_{\rm L} = G_{\rm T} G_{\rm R} \left[\frac{\lambda}{4\pi r} \right]^2 P_{\rm i}$$

where:

 P'_{in} : Input power (prime indicates power due to reflection)

$$P_{m}^{*} = |1 - 1_{T} | P_{m}^{*}$$

$$= |1 - (0.15)^{2} | \times 2$$

$$P_{m}^{*} = 1.955 W$$

$$P_{L} = 63.09 \times 158.48 \left[\frac{\lambda}{4\pi \times 200 \lambda} \right]^{2} \times 1.955$$

$$= 3.1 \times 10^{-3}$$

As there is a reflection at the terminals of Rxing antenna power delivered to the load in given by $P'_L = \left\{ l - \left| \Gamma_R^{-2} \right| \right\} \times P_L$

= {1 − (0.18)²} × 3.1 × 10⁻³ ∴ P'_L = 2.99 mW



64. Ans. C.

Given Electric field of incident wave is $E_w^i = (\hat{a}_x + j\hat{a}_y)E_0e^{jkx}$ $\vec{a} \, z = 0;$ $\vec{E}_w^i = E_0 \cos \omega t \, \hat{a}_x - E_0 \sin \omega t \, \hat{a}_y$ (in time varying form) at $\omega t = 0$ $\vec{E}_w^i = E_0 \hat{a}_x$ $\vec{a} \, \omega t = \frac{\pi}{2}$ $\vec{E}_w^i = E_0(-\hat{a}_y)$

As a tip of electric field intensity is tracing a circle when time varies, hence the wave is said to be circularly polarized in clockwise direction (or) RHCP. Polarizing vector of incident wave is given by,

 $\hat{\mathbf{P}}_{i} = \frac{\hat{\mathbf{a}}_{x} + j\hat{\mathbf{a}}_{y}}{\sqrt{2}}$

radiated electric field from the antenna is

 $\vec{E}_{a} = \left(\hat{a}_{x} + 2\hat{a}_{y} \right) E_{1} \frac{1}{\gamma} e^{-jk\gamma}$

at r = 0

 $\vec{E}_{a}=E_{1}\cos\varpi t \, \hat{a}_{x}+2E_{1}\cos\varpi t \, \hat{a}_{y}$ (in time varying form)

As both x & y components are in-phase, hence the wave is said to be linear polarized. Polarizing vector of radiated field is $\hat{P}_a = \left(\frac{\hat{a}_a + 2\hat{a}_y}{\sqrt{5}}\right)$ polarizing mismatch; The polarizing mismatch is said to have, if the polarization of receiving antenna is not same on the polarization of the incident wave. The polarization loss factor (PLF) characterizes the loss of EM power due to polarization mismatch.

$$PLF = \left| \hat{P}_{i} \cdot \hat{P}_{a} \right|^{2}$$

in dB; PLF (dB) = $10 \log (PLF)$

$$PLF = \left| \left(\frac{\hat{a}_x + j\hat{a}_y}{2} \right) \cdot \left(\frac{\hat{a}_x + 2\hat{a}_y}{\sqrt{5}} \right) \right|^2 = \left| \frac{1 + j2}{\sqrt{2}\sqrt{5}} \right|^2 = \frac{1}{2} (\text{or}) 0.5$$
$$PLF(dB) = 10 \log 0.5 = -3.0102$$

65. Ans. B.

$$P_{rad} = \int_{\theta=0}^{\pi/2} \int_{\phi=0}^{2\pi} W_{rad} r^{2} \sin \theta d\theta d\phi$$

$$= \int_{\theta=0}^{\pi/2} \int_{\phi=0}^{2\pi} \frac{C_{0}}{r^{2}} \cos^{2} \omega r^{2} \sin \omega d\theta d\phi$$

$$= C_{0} \times \frac{-\cos^{2} \theta}{5} \Big|_{0}^{\pi/2} \cdot 2\pi = \frac{2\pi}{5} C_{0} = 1.256C_{0}$$
Max. directivity $= \frac{\max(W_{rad})}{P_{rad}} \times 4\pi r^{2} = \frac{4\pi}{1.256} = 10$
Max. Directivity in $dB = 10 \log 10 = 10 dB$.
